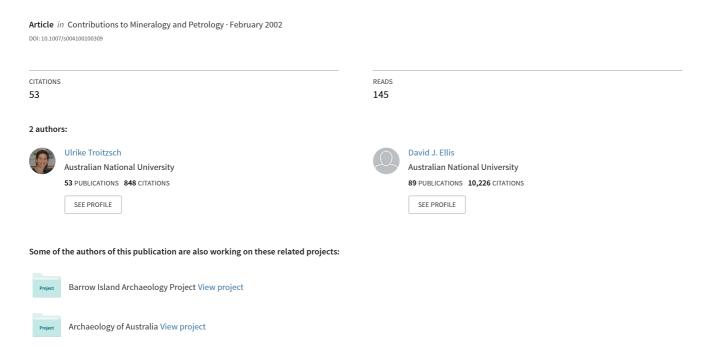
# Thermodynamic properties and stability of AlF-bearing titanite CaTiOSiO 4 - CaAlFSiO 4



Ulrike Troitzsch · David J. Ellis

# Thermodynamic properties and stability of AIF-bearing titanite CaTiOSiO<sub>4</sub>—Ca-AIFSiO<sub>4</sub>

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**Abstract** Calorimetric and experimental data on Alfbearing titanite are presented that yield thermodynamic properties of CaAlFSiO<sub>4</sub>, as well as activity-composition relations of binary titanite CaTiOSiO<sub>4</sub>–CaAlFSiO<sub>4</sub>. The heat capacity of synthetic CaAlFSiO<sub>4</sub> was measured with differential scanning calorimetry between 170 and 850 K:

$$C_P = 689.96 - 0.38647T + 2911300T^{-2} - 8356.1T^{-0.5} + 0.00016179T^2$$

Based on low-temperature heat capacity calculations with lattice vibrational theory (Debye model), the calorimetric entropy of CaAlFSiO<sub>4</sub> can be expected to lie between 104.7 and 118.1 J mol<sup>-1</sup> K<sup>-1</sup>. The temperature of the  $P2_1/a$  to A2/a phase change was determined calorimetrically for a titanite with  $X_{\rm Al}=0.09$  ( $T_{\rm transition}=390$  K). The decrease of the transition temperature at a rate of about 11 K per mol% CaAlFSiO<sub>4</sub> is in good agreement with previous TEM investigations. The displacement of the reaction anorthite + fluorite = CaAlFSiO<sub>4</sub> in the presence of CaTiOSiO<sub>4</sub> was studied with high P–T experiments. Titanite behaves as a non-ideal, symmetrical solid-solution. The thermodynamic properties of CaAlFSiO<sub>4</sub> consistent with a multi-site mixing model are:

Enthalpy of formation (elements) $d_f H^0 = -2740.8 \pm 3.0 \text{ kJmol}^{-1}$ Standard state entropy S<sup>0</sup> =  $104.9 \pm 1.1 \text{ Jmol}^{-1} \text{K}^{-1}$ Margules parameter  $[W_H - TW_s]$  =  $13.6 \pm 0.4 \text{ Jmol}^{-1}$ 

The pressure dependence of the Margules parameter  $(W_V)$  was determined from the excess volume of mixing based on XRD measurements  $(214 \pm 18 \text{ J mol}^{-1} \text{ kbar}^{-1})$ , as well as refined from the piston-cylinder experimental

results  $(198 \pm 114 \text{ J mol}^{-1} \text{ kbar}^{-1})$ , demonstrating consistency between crystal structure data and thermodynamic properties. The stability of AlF-bearing titanite Ca(Ti,Al)(O,F)SiO<sub>4</sub> was investigated by thermodynamic modelling in the system Ca-Al-Si-Ti-O-F-H-C and subsystems. The petrogenetic grids are in good agreement with natural mineral assemblages, in that very Al-rich titanite  $(X_{Al} > 0.65 \pm 0.15)$  is generally absent because it is either unstable with respect to other phases, or its stability field lies outside the P-T conditions realised on Earth. The grids explain both the predominant occurrence of natural Al-rich titanite at high metamorphic grade such as eclogite facies conditions, as well as its scarcity in blueschist facies rocks. Wide spacing of the Al-isopleths for titanite of many high-grade assemblages prevents their use as geobarometers or thermometers. The instability of endmember CaAlFSiO<sub>4</sub> with respect to other phases in most assemblages modelled here is consistent with the hypothesis that the presence of structural stresses in the crystal lattice of CaAlFSiO<sub>4</sub> influences its thermodynamic stability. The titanite structure is not well suited to accommodate Al and F instead of Ti and O, causing the relatively high Gibbs free energy of CaAlFSiO<sub>4</sub>, manifested in its standard state properties. Thus, the increasing amount of CaAlFSiO<sub>4</sub> along the binary join is the reason why titanite with  $X_{\rm Al} > 0.65 \pm 0.15$  becomes unstable in most petrogenetic grids presented here. The compositional limit of natural titanite ( $X_{Al} \approx 0.54$ ) probably reflects the point beyond which the less stable end member begins to dominate the solid-solution, affecting both crystal structure and thermodynamic stability.

#### U. Troitzsch (☑) · D.J. Ellis Department of Geology, Australian National University, Canberra, ACT 0200, Australia E-mail: ulrike@geology.anu.edu.au

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#### Introduction

Titanite (CaTiOSiO<sub>4</sub>) is a common accessory phase in a range of igneous, metamorphic, and some sedimentary rocks. The widespread occurrence of titanite

throughout different geochemical environments and petrogenetic conditions is caused by the large number of other elements that can be substituted into its crystal structure (e.g. Sahama 1946; Oberti et al. 1991). Numerous studies based on natural assemblages, experiments and thermodynamic modelling proposed that titanite is a potential indicator for a range of metamorphic conditions (Kowallis et al. 1997), such as pressure and temperature (Essene and Bohlen 1985; Manning and Bohlen 1991; Mukhopadhyay et al. 1992; Ghent and Stout 1994), fluid composition (Hunt and Kerrick 1977; Valley and Essene 1980; Jacobs and Kerrick 1981; Itaya et al. 1985) and oxygen fugacity (Spear 1981; Wones 1989). Its U-Pb content opens the exciting possibility to date the above metamorphic conditions (Frost et al. 2001). Understanding the stability of titanite in igneous and metamorphic rocks is important because it might play a dominant role in shaping their rare earth element patterns (Hellman and Green 1979, Green and Pearson 1986; Paterson and Stephens 1992; Dawson et al. 1994; Tribuzio et al. 1996). Moreover, the presence or absence of titanite in felsic igneous rocks could be used as an indicator for F contents of magmas (Price et al. 1999).

Because titanite commonly occurs in solid-solution with other end members, it is crucial to understand the mixing behaviour, and activity-composition relations of the most important end members. Although the thermodynamic data of the titanite end member (CaTiOSiO<sub>4</sub>) are known, activity-composition relations of titanite solid-solution had never been determined, so that previous studies assumed either ideal mixing behaviour (Ghent and Stout 1994) or titanite to be pure CaTiOSiO<sub>4</sub> (Mukhopadhyay et al. 1992). Throughout the present paper 'titanite' stands for the phase titanite, thus including solid-solution, whereas pure titanite is referred to as 'end member titanite' or 'CaTiOSiO<sub>4</sub>'.

In the present study we investigated experimentally the activity-composition relations of Al-bearing titanite along the binary join CaTiOSiO<sub>4</sub>-CaAlFSiO<sub>4</sub>, represented by the coupled substitution

$$Ti^{4+} + O^{2-} = Al^{3+} + F^{-}$$
 (1)

The end member CaAlFSiO<sub>4</sub> was chosen for several reasons. First, Al is one of the most common and abundant substituents for Ti in natural titanite, and thus most important for thermodynamic modelling of natural assemblages. Second, among the two main Al end members that occur in natural titanite, i.e. CaAlOHSiO<sub>4</sub> and CaAlFSiO<sub>4</sub>, the latter always dominates in the most Al-rich titanites, but never exceeds 54 mol% (Franz and Spear 1985, Markl and Piazolo 1999). The reasons for this compositional limit were the subject of much discussion (Smith 1981, Oberti et al. 1991). Crystal structure investigations along the join TiO–AlF indicated that, although complete solid-solution is observed, the titanite structure is not well suited

to accommodate  $X_{A1} > 0.5$  (Troitzsch et al. 1999). We examine whether these crystal structural problems are reflected in the thermodynamics of this system, for example as an activity anomaly at this composition. There has been no previous attempt to equilibrate more AlF-rich titanite in a mineralogically buffered phase assemblage. Although Smith (1981) determined qualitatively the dependence of the AlF content in titanite on pressure and temperature with experiments, the equilibrated phase assemblage contained melt and, thus, was not mineralogically buffered, preventing a thorough thermodynamic interpretation of the results. Note, however, the recent study by Tropper et al. (1999, 2000) discussed below. Third, the unit-cell volume of titanite along the binary join TiO-AlF has recently been determined (Troitzsch and Ellis 1999; Troitzsch et al. 1999), permitting accurate thermodynamic calculations with this end member. Fourth, the Al content of titanite is pressure- and temperaturedependent, and thus of special interest for geothermobarometry (Smith 1981; Enami et al. 1993; Franz and Spear 1985).

The potential of Al-bearing titanite in geobarometry has long been recognised (Smith 1980; 1981). Many previous studies of natural (e.g. Franz and Spear 1985; Krogh et al. 1990; Enami et al. 1993; Carswell et al. 1996) and synthetic Al-rich titanite (Smith 1981) have suggested a strong pressure and mild temperature dependence of the Al content in titanite. However, the PTX relationship was never quantified for any assemblage, mainly because of the strong dependence of the system on fluorine, which, until more recently, was difficult to analyse quantitatively with standard equipment.

In the first part of this study we investigated, with differential scanning calorimetry, the heat capacity of synthetic CaAlFSiO<sub>4</sub> required for the subsequent interpretation of high P–T-experiments. Secondly, the  $P2_1/a$  to A2/a phase transition temperature of a synthetic titanite with  $X_{\rm AlF}=0.09$  was determined calorimetrically to improve the resolution of the CaTiO-SiO<sub>4</sub>–CaAlFSiO<sub>4</sub> phase diagram. Thirdly, a series of piston-cylinder experiments was carried out in the system Ca–Ti–Al–Si–O–F, determining the displacement of the reaction

$$0.5$$
CaAl<sub>2</sub>Si<sub>2</sub>O<sub>8</sub> +  $0.5$ CaF<sub>2</sub> = CaAlFSiO<sub>4</sub>  
Anorthite + fluorite = AlF titanite (2)

in the presence of CaTiOSiO<sub>4</sub>. This gave the activity–composition relationship of titanite solid-solution, and the standard state entropy and enthalpy of formation of CaAlFSiO<sub>4</sub>. These thermodynamic data were then used to investigate the stability of AlF-rich titanite.

#### Differential scanning calorimetry details

The heat capacity of CaAlFSiO<sub>4</sub> was determined using the synthetic sample G-297 of Troitzsch and Ellis (1999). This sample contains small amounts of fluorine-rich zoisite, fluorite, and trace

kyanite. As the bulk composition of the sample should be that of CaAlFSiO<sub>4</sub>, and heat capacities of different phases of equivalent composition are similar, the impurities cause only small errors compared with those inherent in the calorimetric equipment and experimental method. The temperature of the  $P2_1/a$  to A2/a phase transition was determined for a titanite with  $X_{\rm AI} = 0.094 \pm 0.008$  (sample AlF09) synthesized at 1,000 °C and 10 kbar from synthetic wollastonite, rutile, anorthite and fluorite (details as in Troitzsch et al. 1999). Sample AlF09 was investigated with SEM and XRD to ensure that only homogeneous titanite was present.

All measurements were carried out with a differential scanning calorimeter DSC 2920 (TA Instruments). Temperature calibrations performed on phase transitions of indium, tin, zinc and  $C_{10}H_8$  indicate an accuracy of  $\pm\,1.5^\circ$  over the temperature range of 353 to 670 K. Non-hermetically sealing aluminium pans were used. Although the calorimetric precision of the instrument is given as 1% by the manufacturer, multiple scans indicated that heat capacities were reproduced to within 2%. Problems encountered during a different set of heat capacity measurements using this calorimeter are described in Troitzsch (2000) who recommended that the heat capacity of CaAlFSiO\_4 be confirmed with a different instrument.

All samples were finely ground in acetone in an agate mortar, and dried. Between 30 and 50 mg of powder was filled into the pans. The lids were inverted in order to compact the powder firmly in the pan, which improves the contact of the sample with the pan bottom and thus with the thermocouple, and facilitates heat transfer in the sample. This was especially important for the transition temperature measurement because it significantly smoothed the trace, probably by limiting movement of grains within the sample during heating. The extremely weak signal of the phase transition would otherwise not have been discerned from background noise. The CaAIFSiO<sub>4</sub> sample was annealed above 800 K for about 30 min to avoid strain-release and recrystallization effects during the run. A sapphire standard was run immediately before each CaAIFSiO<sub>4</sub> sample. Only

the heat flow was determined for sample AlF09. All standard and sample runs were performed at a heating rate of 20° min<sup>-1</sup>, from 170 to 850 K. Two scans of CaAlFSiO<sub>4</sub> were performed, the mean of which was taken as the final value.

#### Piston-cylinder experiments details

Eighteen polybaric runs (1,000 °C) and two sets of polythermal runs (four at 7 kbar, five at 10 kbar) produced AIF-bearing titanite in the assemblage titanite–anorthite–fluorite (Table 1). The starting mixes of binary titanite composition ( $X_{\rm AI}$  = 0.60 to  $X_{\rm AI}$  = 0.96) were composed of synthetic anorthite, wollastonite, fluorite (Specpure), and TiO<sub>2</sub> (Degussa). The synthesis of anorthite and wollastonite from glass was described in Troitzsch and Ellis (1999) and Troitzsch et al. (1999). 2-mm diameter Ag<sub>0.75</sub>Pd<sub>0.25</sub> capsules were filled with the starting powder, dried for at least 2 h at 110 °C, and then welded shut. Experimental procedure was as described in Troitzsch et al. (1999). An error of  $\pm$ 0.2 kbar of all pressure readings, and  $\pm$ 5 °C with respect to temperature, was used in the curve fitting procedure.

One set of reversal experiments was carried out at 10 kbar, re-equilibrating run products of samples G-395 and G-398, previously run at 12 and 8 kbar, respectively (Table 1). Each sample was reground, filled in a 2-mm diameter Ag<sub>0.75</sub>Pd<sub>0.25</sub> capsule, dried and welded shut. Both capsules were then placed next to each other in the same pressure assembly and run in one experiment to ensure identical pressure and temperature conditions. The second set of reversals consisted of samples G-407 and G-411, formerly equilibrated at 17 and 14 kbar, which were re-run at 15.5 kbar.

The run products were investigated with reflected light microscopy, X-ray diffraction and scanning electron microscopy. Although in high-temperature runs (>900  $^{\circ}$ C) the grain-size of the products (<10  $\mu$ m) enabled the determination of the titanite

**Table 1** Run conditions and results of piston-cylinder experiments. *An* Anorthite; *Fluo* fluorite; *Gro* grossular; *Ttn* titanite; *Zoi* zoisite

TD.	D.	, a	17	D 1 .	17	CD II
-	-	-		Kun products		$SD X_{Al}$
(°C)	(Kbar)	(n)	IVIIX		1 tn	
1,000	5	70	0.60	Ttn An Fluo	0.282	0.007
1,000	5	71	0.60	Ttn An Fluo	$0.282^{b}$	0.004
1,000	6	70	0.60	Ttn An Fluo	$0.290^{\rm b}$	0.004
800	7	504	0.60	Ttn An Fluo	$0.393^{\rm b}$	0.004
850	7	192	0.80	Ttn An Fluo	$0.371^{\rm b}$	0.004
950	7	72	0.60	Ttn An Fluo	$0.330^{b}$	0.004
1,000	7	58	0.60	Ttn An Fluo	$0.309^{b}$	0.004
1,000	8	50	0.60	Ttn An Fluo	0.340	0.011
1,000	9	70	0.60	Ttn An Fluo	0.367	0.005
800	10	480	0.60	Ttn An Fluo Gro <sup>c</sup>	0.519 <sup>b</sup>	0.004
850	10	480	0.60	Ttn An Fluo	0.471	0.005
900	10	71	0.60	Ttn An Fluo	$0.460^{b}$	0.004
950	10	71	0.60	Ttn An Fluo	0.417	0.014
1,000	10	50	0.60	Ttn An Fluo	0.394	0.012
1,000	11	70	0.60	Ttn An Fluo	0.422	0.009
1,000	11	71	0.60	Ttn An Fluo	0.427	0.019
1,000	12	36	0.60	Ttn An Fluo	0.464	0.016
1,000	13	68	0.60	Ttn An Fluo	0.487	0.013
1,000	14	44	0.84	Ttn An Fluo	0.563	0.014
1,000	15	79	0.84	Ttn An Fluo Zoi <sup>c</sup>	0.605	0.012
1,000	15.5	44	0.84	Ttn An Fluo	0.612	0.011
1,000	16	58	0.80	Ttn An Fluo Zoi <sup>c</sup>	0.632	0.014
1,000	17	51	0.84	Ttn An Fluo	0.679	0.013
1,000	20	67	0.96	Ttn An Fluo	$0.816^{b}$	0.004
1,000	21	69	0.96	Ttn An Fluo Zoi <sup>c</sup>	0.914 <sup>b</sup>	0.004
	1,000 1,000 800 850 950 1,000 1,000 800 850 900 950 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	(°C) (kbar)  1,000 5 1,000 5 1,000 6 800 7 850 7 950 7 1,000 8 1,000 9 800 10 850 10 950 10 1,000 11 1,000 11 1,000 11 1,000 12 1,000 13 1,000 14 1,000 15 1,000 15 1,000 15 1,000 15 1,000 15 1,000 15 1,000 17 1,000 20	(°C) (kbar) (h)  1,000 5 70 1,000 5 71 1,000 6 70 800 7 504 850 7 192 950 7 72 1,000 8 50 1,000 8 50 1,000 9 70 800 10 480 850 10 480 900 10 71 1,000 10 50 1,000 11 70 1,000 12 36 1,000 13 68 1,000 14 44 1,000 15 79 1,000 15 79 1,000 15 79 1,000 16 58 1,000 16 58 1,000 17 51 1,000 16 58 1,000 17 51 1,000 17 51 1,000 16 58 1,000 17 51 1,000 16 58 1,000 17 51 1,000 17 51 1,000 17 51 1,000 17 51 1,000 17 51 1,000 17 51 1,000 17 51	(°C) (kbar) (h) Mix  1,000 5 70 0.60 1,000 5 71 0.60 1,000 6 70 0.60 800 7 504 0.60 850 7 192 0.80 950 7 72 0.60 1,000 8 50 0.60 1,000 8 50 0.60 1,000 9 70 0.60 800 10 480 0.60 850 10 480 0.60 950 10 71 0.60 950 10 71 0.60 1,000 10 50 0.60 1,000 11 70 0.60 1,000 11 71 0.60 1,000 12 36 0.60 1,000 13 68 0.60 1,000 14 44 0.84 1,000 15 79 0.84 1,000 16 58 0.80 1,000 17 51 0.84 1,000 16 58 0.80 1,000 17 51 0.84 1,000 17 51 0.84 1,000 17 51 0.84 1,000 17 51 0.84 1,000 17 51 0.84 1,000 17 51 0.84 1,000 17 51 0.84 1,000 17 51 0.84 1,000 17 51 0.84 1,000 17 51 0.84	(°C) (kbar) (h) Mix  1,000 5 70 0.60 Ttn An Fluo 1,000 6 70 0.60 Ttn An Fluo 1,000 6 70 0.60 Ttn An Fluo 800 7 504 0.60 Ttn An Fluo 850 7 192 0.80 Ttn An Fluo 1,000 7 58 0.60 Ttn An Fluo 1,000 7 58 0.60 Ttn An Fluo 1,000 8 50 0.60 Ttn An Fluo 1,000 9 70 0.60 Ttn An Fluo 1,000 9 70 0.60 Ttn An Fluo 1,000 9 70 0.60 Ttn An Fluo 800 10 480 0.60 Ttn An Fluo 850 10 480 0.60 Ttn An Fluo 900 10 71 0.60 Ttn An Fluo 900 10 71 0.60 Ttn An Fluo 1,000 10 50 0.60 Ttn An Fluo 1,000 11 70 0.60 Ttn An Fluo 1,000 11 70 0.60 Ttn An Fluo 1,000 11 70 0.60 Ttn An Fluo 1,000 12 36 0.60 Ttn An Fluo 1,000 13 68 0.60 Ttn An Fluo 1,000 14 44 0.84 Ttn An Fluo 1,000 15 79 0.84 Ttn An Fluo 1,000 15 79 0.84 Ttn An Fluo 1,000 16 58 0.80 Ttn An Fluo 1,000 17 51 0.84 Ttn An Fluo 1,000 17 51 0.84 Ttn An Fluo 1,000 17 51 0.84 Ttn An Fluo	(°C)         (kbar)         (h)         Mix         Ttn           1,000         5         70         0.60         Ttn An Fluo         0.282           1,000         5         71         0.60         Ttn An Fluo         0.282b           1,000         6         70         0.60         Ttn An Fluo         0.290b           800         7         504         0.60         Ttn An Fluo         0.393b           850         7         192         0.80         Ttn An Fluo         0.371b           950         7         72         0.60         Ttn An Fluo         0.330b           1,000         7         58         0.60         Ttn An Fluo         0.309b           1,000         8         50         0.60         Ttn An Fluo         0.340           1,000         9         70         0.60         Ttn An Fluo         0.347           800         10         480         0.60         Ttn An Fluo Groc         0.519b           850         10         480         0.60         Ttn An Fluo         0.471           900         10         71         0.60         Ttn An Fluo         0.460b           950         10

<sup>&</sup>lt;sup>a</sup>Run duration

<sup>&</sup>lt;sup>b</sup>Al content determined only with XRD via unit cell dimensions. Standard deviations of these values as given in the last column represent the estimated mean error of this method. All other values determined with SEM

<sup>&</sup>lt;sup>c</sup>Trace amounts

composition with SEM, at lower temperatures the grain-size  $(<2 \mu m)$  approached the analytical resolution limit of the SEM. Therefore, the AIF content of titanite in the latter as well as for some high temperature runs was determined indirectly via the unitcell dimensions a, b and c of titanite, which were obtained from powder X-ray diffraction patterns using the Rietveld refinement computer program RIETAN (Izumi 1993; Kim and Izumi 1994). The change in unit-cell dimensions of synthetic titanite along the binary join CaTiOSiO<sub>4</sub>-CaAlFSiO<sub>4</sub> are given in the Appendix, based on Troitzsch et al. (1999). The accuracy of this method was tested with several high temperature run products, which were coarse-grained and thus yielded reliable SEM analyses. Figure 1 shows that the AlF content obtained with XRD reproduces the mean of the SEM analyses of each sample with a precision of  $X_{\rm A1} \pm 0.004$ , demonstrating the consistency of both methods, and the accuracy of the polynomial functions in the Appendix.

Quantitative analyses were obtained with a JEOL JSM-6400 scanning electron microscope with attached Si(Li) detector, Link ISIS EDS, at 15 kV and 1 nA. Analyses were calculated using a ZAF correction. Analysed elements were silicon (standard: SiO<sub>2</sub>), titanium (TiO<sub>2</sub>), aluminium and oxygen (albite), calcium (diopside) and fluorine (fluorite). The determination of the number of atoms per formula unit is based on three total cations (Franz and Spear 1985) instead of anion-based calculations because it avoids the propagation of large errors attached to the F-analyses (6%, as opposed to 1.0, 1.1, 0.6, 0.7 and 1.3% for oxygen, aluminium, silicon, calcium and titanium, respectively). A minimum of 10 titanite grains was analysed per sample. Apart from a slight Si deficiency of about 0.01 a.p.f.u., and a small surplus of Ca of about 0.02 a.p.f.u., the analyses suggest ideal occupation on all sites. Therefore, the amount of CaAlFSiO<sub>4</sub> was calculated as  $X_{Al} = Al/(Al + Ti)$ .

The interpretation of the experimental results [reaction (2)] was based on thermodynamic data of anorthite from Berman (1988), and fluorite from Robie and Hemingway (1995). Thermal expansion (Carmichael 1984) and isothermal compressibility of fluorite (Birch 1966) were transformed to suit the volume equation of Berman (1988) used in the regression. The molar volume of Ca-AlFSiO<sub>4</sub> was taken from Troitzsch et al. (1999). Expansion and compressibility of CaAlFSiO<sub>4</sub> were assumed to be identical to those of titanite, which were estimated based on the high pressure XRD data of Angel et al. (1999), and the high temperature studies of Taylor and Brown (1976) and Ghose et al. (1991). The pressure dependence of the Margules parameter  $(W_V = 214.08 \pm 18 \text{ J kbar}^{-1})$  was calculated from the excess volume

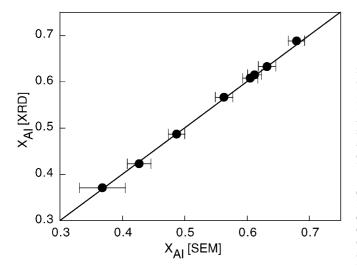


Fig. 1 The Al-content of synthetic titanite  $(X_{Al})$  determined via the unit-cell dimensions with X-ray diffraction (XRD), versus electron microprobe (SEM) data of the same samples. Solid line represents ideal correlation. Error bars in  $X_{Al}$  (SEM) are the standard deviation of the microprobe data

of mixing determined by Troitzsch et al. (1999). Only data with  $X_{\rm Al} > 0.09$  were used, allowing a symmetrical fit to the data. The enthalpy of formation and entropy of CaAlFSiO<sub>4</sub>, and the Margules parameter term  $(W_H - TW_S)$  were determined by free-energy minimization, fitting the experimental PTX<sub>Al</sub> data to

$$\Delta G = 0 = \Delta H_{1,298}^{0} + \int_{298}^{T} C_{P} dT - T \Delta S_{1,298}^{0} - T \int_{298}^{T} \frac{C_{P}}{T} dT + \int_{1}^{P} \Delta V dP + RT \ln K$$
(3)

Two activity models were used. The multi-site mixing (MM) model assumes independent distribution of Al and F on each site,

$$RT \ln a_{CaAlFSiO_4}^{Tin} = 2RT \ln X_{Al} + (W_H - TW_S + PW_V)(1 - X_{Al})^2$$
 (4)

Here, the Margules parameters are a combination of the Margules parameters for each site  $[W_X = (W_X)_{T_{i-}Al} + (W_X)_{O-F}]$ . The local charge balance (LCB) model is described by

$$RT \ln a_{CaAlFSiO_4}^{Tin} = RT \ln X_{Al} + (W_H - TW_S + PW_V)(1 - X_{Al})^2$$
 (5)

Least squares regression of the experimental  $PTX_{Al}$  data-triplets was carried out with a BASIC program of Hugh O'Neill. This program performs a Gauss-Jordan matrix inversion, as described in Miller (1981), weighting each data point according to its errors.

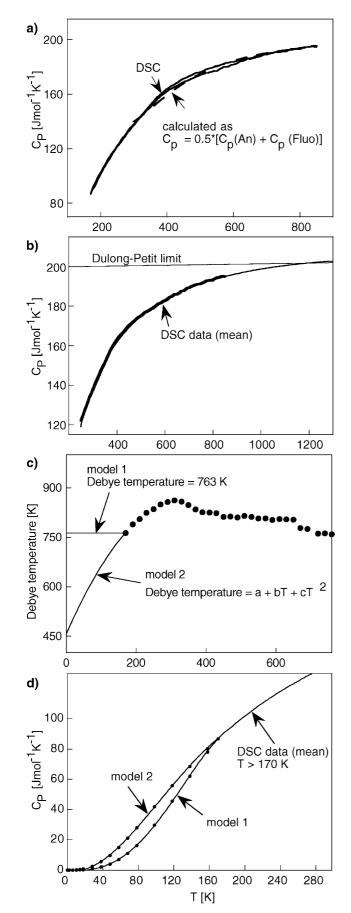
#### **Modelling details**

Four types of reaction with Al-rich titanite are considered (non-stoichiometric, and with unspecified additional product and reactant phases):

- Fluid-absent:
  - 1. Reactants + fluorite = products + CaAlFSiO<sub>4</sub>
- Fluid-present:
  - 2. Reactants + hydrous phase + fluorite = products +  $CaAlFSiO_4 + H_2O$
- 3. Reactants + carbonate + fluorite = products +  $CaAlFSiO_4 + CO_2$ 4. Reactants +  $F_2$  = products +  $CaAlFSiO_4 + O_2$

A binary H<sub>2</sub>O–CO<sub>2</sub> fluid is assumed for reactions of types 2 and 3. Ignoring the fluid species HF and F<sub>2</sub> in such equilibria is common practice (e. g. Rice 1980; Barton 1982), as the concentrations of HF and F<sub>2</sub> in metamorphic fluids are extremely low (Munoz and Eugster 1969; Rice 1980; Valley et al. 1982; Droll and Seck 1984; Haselton et al. 1988; Webster and Holloway 1990; Aksyuk and Zhukovskaya 1994). Because HF and F<sub>2</sub>, however, do affect the stability of F-bearing phases (e.g. Bohlen and Essene 1978), by analogy to the strong effect oxygen has on many phase equilibria despite its extreme dilution, the effect of F<sub>2</sub> on the stability of AlFbearing titanite is investigated with reactions of type 4.

The equilibria and titanite  $X_{Al}$ -contours were calculated by free energy minimization using the relationships (3) and (4), adopting the MM model for titanite. The equilibria were computed using the calculation methods and data of Berman (1988) for all phases, except for fluorite, CaAlFSiO<sub>4</sub>, and H<sub>2</sub>O below 10 kbar. Fluorite data were taken from Robie and Hemingway (1995), with expansion and compressibility terms from Carmichael (1984) and Birch (1966), respectively. The activity of grossular was calculated with the model of Berman (1990). Fugacities of CO<sub>2</sub>, H<sub>2</sub>O-CO<sub>2</sub> mixtures and H<sub>2</sub>O (below 10 kbar) were calculated with the modified Redlich-Kwong equation proposed by Kerrick and Jacobs (1981). Water fugacities above 10 kbar were computed with the empirical equation of Delany and Helgeson (1978). The fluid pressure equals total pressure.



Substitution of F<sup>-</sup> for OH<sup>-</sup> in hydrous minerals was not considered, and all phases were assumed to be the respective OH end member. Although zoisite in the experiments of Troitzsch and Ellis (1999) contained considerable amounts of fluorine, the assumption that it is F-free in the calculations is justified given that natural zoisite does not seem to incorporate much fluorine even in F-rich rocks (Makanjuola and Howie 1972; López Sánchez-Vizcaíno et al. 1997).

#### Heat capacity of CaAIFSiO<sub>4</sub>

The experimentally determined specific heat of CaAlF-SiO<sub>4</sub> increases smoothly with temperature (Fig. 2a). Both scans deviate less than 3% from the sum of the published heat capacities of anorthite and fluorite. The experimental data are reproduced to within 1% (between 170 and 850 K) by

$$C_P(\text{Jmol}^{-1}\text{K}^{-1}) = 689.96 - 0.38647T + 2911300T^{-2} - 8356.1T^{-0.5} + 0.00016179T^2$$
 (6)

The thermodynamic interpretation of the piston-cylinder run products requires the extrapolation of the CaAlFSiO<sub>4</sub> heat capacity data to the experimental temperatures (1,073 to 1,273 K). Because no melting was observed in the run products, the heat capacity of CaAlFSiO<sub>4</sub> was assumed to increase smoothly beyond 850 K to at least 1,273 K, slowly approaching the 'Dulong-Petit limit' (Gopal 1966; Berman and Brown 1985). The latter was calculated with expansion and compressibility data from Table 2. Figure 2b shows the extrapolation of the heat capacity data (250 to 850 K) to 1,300 K, with an extended Maier and Kelley (1932) heat capacity polynomial (Haas and Fisher 1976)

$$C_P(\text{Jmol}^{-1}\text{K}^{-1}) = 272.54 - 0.01319T - 2055700T^{-2} - 1854.4T^{-0.5}$$
(7)

Two dummy points on the DPL at 1,500 K and 1,800 K were included in the fitting procedure, to ensure that the heat capacity smoothly approaches the theoretical limit. A satisfactory fit to the experimental data

•

**Fig. 2 a** Heat capacity  $C_P$  of synthetic CaAlFSiO<sub>4</sub> determined with differential scanning calorimetry in two scans (*solid lines*), and estimated from the heat capacities of anorthite (*An*) and fluorite (*Fluo*) (*dashed line*). **b** Extrapolation of experimental heat capacity (DSC data) to 1,300 K with Eq. (9) in the text. The calculation of the Dulong-Petit limit is described in the text. C Variation of the Debye temperature of CaAlFSiO<sub>4</sub> with temperature. Debye temperatures calculated from calorimetric data above 170 K (*dots*) were extrapolated to absolute zero with two methods (*solid lines*) discussed in the text. Polynomial coefficients of model 2: a = 456.25, b = 2.4175,  $c = -3.5535 \times 10^{-3}$ . **d** Low-temperature heat capacity of CaAlFSiO<sub>4</sub> (*dots*, T < 170 K) calculated with the extrapolated Debye temperatures of **c**, and experimental heat capacity (*solid line*, T > 170 K). Polynomial functions  $y = a + bT + cT^2 + dT^3 + eT^4$  were fitted to the data points between 0 and 170 K (*solid lines*). Model 1 a = 0.17015, b = -0.02873, c = 0.00042236,  $d = 4.18116 \times 10^{-5}$ ,  $e = -1.8851 \times 10^{-7}$ ; model 2 a = 0.5119, b = -0.1602, c = 0.0092202,  $d = -3.7612 \times 10^{-5}$ ,  $e = 3.7772 \times 10^{-8}$ 

**Table 2** Thermodynamic properties of CaAlFSiO<sub>4</sub>, determined with Piston-cylinder experiments (Exp.), X-ray diffraction (XRD) and differential scanning calorimetry (DSC). Lower part of the table shows values used in the data regression, upper part shows results. The calculation of the Gibbs energy of formation was based on the data for the elements of Robie and Hemingway (1995). The regression resulted in  $\gamma^2 = 0.67$  and  $\chi^2 = 1.10$  for the MM and LCBmodel, respectively

Property					Method
MM model Gibbs energy Enthalpy Entropy Margules parameter	$d_fG^0$ $d_fH^0$ $S^0$ $W_{H^-}TW_S$	-2,592.9 -2,740.8 104.9 13.6	$\pm 1.8 \\ \pm 3.0 \\ \pm 1.1 \\ \pm 0.5$	kJ mol <sup>-1</sup> kJ mol <sup>-1</sup> J mol <sup>-1</sup> K <sup>-1</sup> J mol <sup>-1</sup>	Exp. Exp. Exp.
LCB model Gibbs energy Enthalpy Entropy Margules parameter	$egin{aligned} d_f G^0 \ d_f H^0 \ S^0 \ W_{H^+} & \mathrm{T} W_S \end{aligned}$	-2,587.8 -2,733.8 111.3 -9.1	$\pm 1.8 \\ \pm 3.1 \\ \pm 1.2 \\ \pm 0.4$	kJ mol <sup>-1</sup> kJ mol <sup>-1</sup> J mol <sup>-1</sup> K <sup>-1</sup> J mol <sup>-1</sup>	Exp. Exp. Exp.
Margules parameter Molar volume Compressibility Expansion	$W_V$ $V^a$ $v_1$ $v_2$ $v_3$ $v_4$	$214 \\ 5.183 \\ -9.29 \times 10^{-7} \\ 2.754 \times 10^{-12} \\ 1.820 \times 10^{-5}$	±18	kJ bar <sup>-1</sup> J mol <sup>-1</sup> bar <sup>-1</sup> bar <sup>-2</sup> K <sup>-1</sup> K <sup>-2</sup>	XRD XRD b b b
Heat capacity	$egin{array}{c} C_P & a \\ b & c \\ d & \end{array}$	272.54 -0.01319 -2,055,700 -1,854.4		J mol <sup>-1</sup> J mol <sup>-1</sup> K <sup>-1</sup> J mol <sup>-1</sup> K <sup>2</sup> J mol <sup>-1</sup> K <sup>0.5</sup>	DSC DSC DSC DSC

<sup>&</sup>lt;sup>a</sup>Troitzsch et al. (1999)

was obtained by allowing the curve to slightly exceed the DPL at higher temperatures (Fig. 2b).

#### Calorimetric entropy of CaAlFSiO<sub>4</sub>

The calorimetric entropy of a phase at standard state (1 bar, 298.15 K) can be calculated if its heat capacity is known between 0 K and 298.15 K. Because CaAlFSiO<sub>4</sub> heat capacity data are limited to above 170 K, they were extrapolated to 0 K with first principle calculations based on vibrational theory, using the Debye model (e.g. Gopal 1966). Two alternative extrapolations of the Debye temperature to 0 K were considered, in order to cover the entire possible range for entropy values. Model 1 assumes the Debye temperature of 763 K, calculated for the lowest temperature data point, remains constant between 0 and 170 K. Model 2 extrapolates the drop-off in the Debye temperature with a 2nd degree polynomial function fitted to DSC data between 170 and 300 K

(Fig. 2c). Figure 2d shows the low temperature heat capacities calculated with these two models. Polynomial functions fitted to the 16 data points of each model yielded the entropy contribution  $S_{170}$  from the temperature range 0 to 170 K (Table 3). This was then added to the entropy contribution from 170 to 298 K, obtained from Eq. (6). Because of the sensitivity of the entropy to small errors in the heat capacity at low temperatures, these calculated values should be treated as best possible maximum/minimum estimates for the calorimetric entropy of CaAlFSiO<sub>4</sub>. Assuming there is neither a low temperature heat capacity anomaly (e.g. caused by a phase transition) nor a configurational contribution to the entropy, the calorimetric entropy (Table 3) can be taken as a first estimate for the standard state entropy of CaAlFSiO<sub>4</sub>.

An alternative way to estimate the standard state entropy of an unknown substance is to sum the entropies of its components, taking into account any volume or co-ordination differences between the phase and its

Table 3 Estimates of calorimetric entropy of CaAlFSiO<sub>4</sub> based on DSC measurements (models 1 and 2, see text and Fig. 2), and on entropies of the components. Entropy values from high P–T experiments are shown for comparison

Method	$S_{170} = \int\limits_{0}^{170} rac{C_{p}}{T} dT$	$S_{298} - S_{170} = \int\limits_{170}^{298} \frac{C_p}{T} dT$	$S_{298}^0 = \int\limits_0^{298} \frac{C_p}{T} dT$
	Debye model	Calorimetry	
	$(J \text{ mol}^{-1} \text{ K}^{-1})$	$(J \text{ mol}^{-1} \text{ K}^{-1})$	(J mol <sup>-1</sup> K <sup>-1</sup> )
Debye (model 1)	41.5	63.2	104.7
Debye (model 2)	54.9	63.2	118.1
Sum of components	Fyfe et al. (1958)		112.9
•	Holland (1989)		120.1
High P-T experiments	MM model		104.9
	LCB model		111.3

<sup>&</sup>lt;sup>b</sup>Assumed to be equal to respective values for titanite:  $v_1$  and  $v_2$  based on Angel (1999);  $v_3$  and  $v_4$  based on Ghose et al. (1991) and Taylor and Brown (1976)

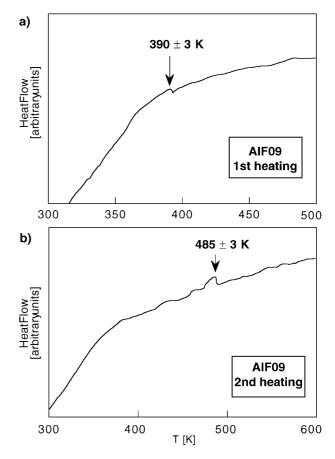
constituents. Choosing anorthite and fluorite as components (data from Robie and Hemingway 1995), and based on the method by Fyfe et al. (1958) with volume correction, the entropy of CaAlFSiO<sub>4</sub> results in  $112.9\pm0.3~\mathrm{J~mol^{-1}~K^{-1}}$ . This value lies within the entropy range estimated from combined DSC and first principle calculations (Table 3). The method by Holland (1989), which besides volume changes, accounts for coordination differences between Al in anorthite and CaAlFSiO<sub>4</sub>, results in a value of 120.1 J mol<sup>-1</sup> K<sup>-1</sup>, similar to our Debye extrapolation model 2.

### **Transition temperature**

The the  $P2_1/a$  to A2/a phase transition in pure titanite takes place at about 496 K, as indicated by Raman spectroscopy (Salje et al. 1993), TEM (Van Heurck et al. 1991), XRD (Ghose et al. 1991; Chrosch et al. 1997), and infrared spectroscopy (Meyer et al. 1998). Calorimetric studies by Zhang et al. (1995) and Xirouchakis and Tangeman (1998) reported lambda-shaped anomalies at 486 and  $483 \pm 5$  K, respectively, which probably represent the phase transition. Because this phase change takes place in several steps over a certain temperature interval, it is necessary to define which part of the transition is determined here. According to Kek et al. (1997), the onset of the phase transition in pure titanite at 496 K is characterized by the displacement of the Ti atom. This induces anti-phase domain formation, and thus the loss of long-range order within each octahedral chain that characterizes the low temperature phase  $\alpha$  with space group  $P2_1/a$ . Between 496 and 825 K the intermediate phase  $\beta$  is stable (Ca atom on splitposition). Titanite with true A2/a symmetry, phase  $\gamma$ , exists above 825 K (Ca atom oscillates between two positions). The most energetic part of this stepwise phase change is its onset at 496 K, which is, therefore, determined in this study. For the sake of consistency with most previous studies, this onset will be termed the  $P2_1/a$ to A2/a 'phase transition', or 'phase change', bearing in mind that it probably does not strictly represent the entire  $P2_1/a$  to A2/a transformation.

The transition temperature should drop with increasing AIF-content in titanite, reaching room-temperature somewhere between 9 and 18.2 mol% of CaAIFSiO<sub>4</sub>, as indicated by TEM investigations of previous studies (Troitzsch et al. 1999, and references therein). Measuring the transition temperature of a sample with  $X_{\rm AI} = 0.09$  with DSC tested the detection limit of the calorimeter because the transition enthalpy of the titanite phase change is very small ( $\sim 80~\rm J~mol^{-1}$ , Thiéblot et al. 1999). Moreover, the well-defined lambda-shaped anomaly in the heat capacity of pure titanite (Zhang et al. 1995) can be expected to broaden and 'smear out' with increasing 'impurities' (Meyer et al. 1998) such as Al.

The first heating ramp produced a signal at about 390 K, consistent with a drop in transition temperature as Al increases (Fig. 3a). However, this signal was not



**Fig. 3** Heat flow measurement (not converted to absolute heat capacity data; units therefore arbitrary) of sample AlF09. In the light of other methods discussed in the text, the signal detected with the first scan **a** is interpreted to represent the  $P2_1/a$  to A2/a phase transition of titanite with  $X_{\rm Al} = 0.09$ . The signal in the second scan **b** is identical to that of pure titanite, possibly suggesting unmixing of the sample into Al-free and Al-enriched domains

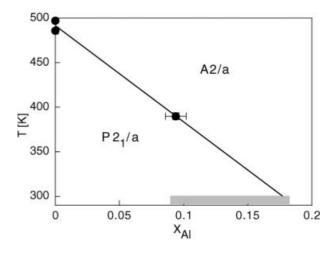


Fig. 4 Section of the phase diagram CaTiOSiO<sub>4</sub>–CaAlFSiO<sub>4</sub>, which covers the  $T-X_{Al}$  range of the  $P2_1/a$  to A2/a phase transition, based on thermal anomalies detected in pure titanite (Salje et al. 1993; Zhang et al. 1995) and sample AlF09 (this study). Shaded area represents  $X_{Al}$  range of the phase transition at room temperature, based on TEM studies

detected during the second heating of the same sample, where a different signal at 485 K showed instead (Fig. 3b), i.e. the transition temperature observed in end member titanite (Xirouchakis and Tangeman 1998). This may indicate that the Al-bearing sample is exsolving domains of pure titanite composition during multiple heating and cooling. We do not know at this point whether the inferred Al-rich domains in the sample crystallise with the titanite structure or as a different phase.

Figure 4 shows the titanite phase diagram at low Al contents, based on the transition temperature of pure titanite (Salje et al. 1993; Zhang et al. 1995) and sample AlF09. Linear extrapolation of the phase boundary to room temperature predicts the phase change to occur at  $X_{\rm Al} = 0.179$ , consistent with the range of  $X_{\rm Al} = 0.09$  and 0.182 indicated by previous TEM investigations (Troitzsch et al. 1999). The extrapolation of the transition temperature to 0 K yields a transition composition of  $X_{\rm Al} = 0.455$ , indicating that the end member CaAlFSiO<sub>4</sub> probably lies in the A2/a stability field at all temperatures. This is consistent with the assumption made in the above Debye model calculations, of the absence of any low-temperature heat-capacity anomalies.

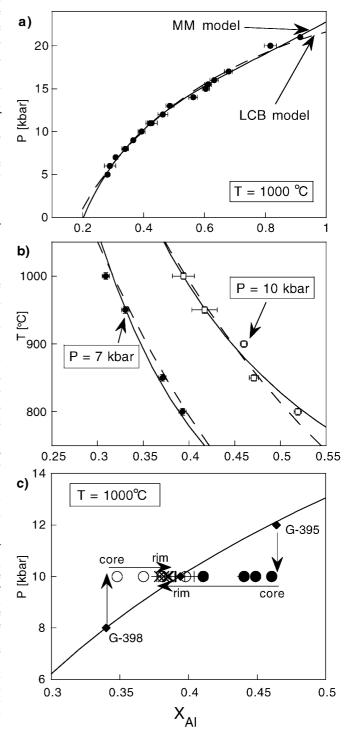
# High P–T experiments and thermodynamic properties of $CaAIFSiO_4$

All run products were composed of anorthite, fluorite and titanite, with or without trace grossular or F-rich zoisite (Table 1).  $X_{\rm Al}$  of titanite increases with pressure, but decreases with temperature (Fig. 5a, b), qualitatively confirming the experiments of Smith (1981). However, although  $X_{\rm Al}$  in Smith's (1981) assemblage titanite—corundum—rutile—melt did not increase beyond 0.54, but instead levelled out at that value,  $X_{\rm Al}$  of titanite coexisting with anorthite and fluorite in this study ranges from 0.282 to 0.914, and even increases more strongly at high pressure.

The generally smooth increase of  $X_{A1}$  with pressure is interrupted by a small irregularity between  $X_{A1}$  of 0.49 and 0.61 (Fig. 5a). This could reflect underlying crystal structure processes, such as the atomic rearrangement in titanite at this composition (Troitzsch et al. 1999) with

Fig. 5a-c High P-T experimental results. a Pressure and b temperature dependence of the Al-content  $(X_{Al})$  of titanite coexisting with anorthite and fluorite. Solid and dashed lines represent the thermodynamic interpretation of the experimental results with a multi-site mixing (MM) model and local charge balance (LCB) model, respectively (data of Table 2). c Titanite composition of two reversal experiments (large symbols) compared with previous runs (small symbols, and solid line). Starting materials of the reversals are characterised by their run number (e.g. G-398, Table 1). Vertical arrows indicate pressure difference between previous and reversed runs. Horizontal arrows indicate changes in composition from core (circles) to rim (crosses) of titanite grains in the reversal runs. Reversal of G-395 is shown as solid circles and upright crosses, G-398 as open circles and diagonal crosses

its potential effect on the activity. However, the anomaly is within the range of experimental error, and should be noted, but not over-interpreted. Thus, a significant thermodynamic expression of the crystal structural problems at  $X_{\rm Al} > 0.6$  identified by Troitzsch et al. (1999) does not exist in the activity–composition relations. Compare, for example, the anomaly observed in the activity of jadeitic pyroxenes, which can be related to ordering processes and change in space group (Holland 1983).



All run products of the reversal experiments consisted of anorthite, fluorite and titanite. The titanites were zoned, with cores comparable to the titanite composition of the previously equilibrated run, and the rims approaching the Al content as determined by the main runs at each pressure (Fig. 5c). These 'intermediate' Al contents were approached from both sides, suggesting that the main runs represent near-equilibrium conditions. Because of the compositional zoning of titanites, the reversal experiments were not used in the data regression.

The thermodynamic data of CaAlFSiO<sub>4</sub> and the Margules parameter term ( $W_H$ – $TW_S$ ) obtained from PTX<sub>Al</sub>-data regression with Eq. (3) are listed in Table 3 (see the Appendix for results referring to different databases). Solid and dashed lines in Fig. 5a, b represent the MM model [Eq. (4)] and LCB-model [Eq. (5)], re#132;spectively. Neither the refinement of asymmetrical Margules parameters, nor the temperature-dependent parameter  $W_S$ , improved the regression result for either model, but instead produced unreasonably large errors.

Both mixing models represent the experimental data well, with a slightly smaller  $\chi^2$  and therefore better fit for the MM model. For example, at high pressures the LCBmodel fails to match the two most aluminous data points (Fig. 5a). The fact that  $\chi^2 > 1$  for the MM model indicates that some of the errors used in the data regression are possibly overestimated. The uncertainty of the temperature readings of  $\pm 5$  °C is unlikely to be any smaller. However, if the error of the pressure readings was only half of that assumed here ( $\pm 0.2$  kbar), then  $\chi^2$  would be close to unity for the MM model, and respectively higher for the LCB model. Also, it is likely that those errors of  $X_{A1}$  are overestimated, which are represented by the standard deviation of SEM analyses (Table 2). If these errors were, for example, only based on the accuracy of SEM analyses (Al ± 1.1 wt%,  $Ti \pm 1.3$  wt%), and applied to the average  $X_{A1}$  of each sample  $(X_{A1} \pm 0.06)$ , then  $\chi^2$  would approach unity, and be respectively larger for the LCB model. Multi-site mixing requires a more negative standard state enthalpy and smaller entropy of CaAlFSiO<sub>4</sub> than does molecular mixing (Table 2).

The standard state entropies derived for both mixing models lie within the entropy range determined by calorimetry (Table 3), suggesting no significant additional entropy contributions (e.g. configurational entropy or low T-phase transition). Figure 6 shows the Al content of titanite in the divariant assemblage anorthite–fluorite–titanite, calculated with the Table 2 data. Open diamonds are recent results of Tropper et al. (1999, 2000), indicating run-conditions at which AIF-bearing titanite was equilibrated with anorthite and fluorite (± rutile) in piston-cylinder experiments. The good agreement of their data with the predicted Al contents in Fig. 6 demonstrates reproducibility of our experiments, as well as the reliability of the derived thermodynamic properties presented here.

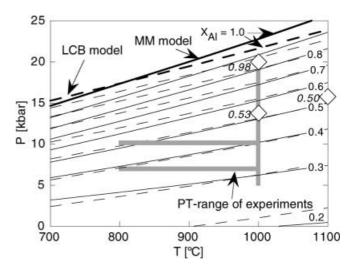


Fig. 6 AIF-content of titanite  $(X_{\rm AI})$  in the divariant assemblage anorthite–fluorite–titanite solid-solution, as predicted by the MM and LCB-model. *Open diamonds* are recent experimental results by Tropper et al. (1999, 2000), indicating run conditions at which titanite was equilibrated with anorthite and fluorite, with or without rutile. The titanite composition they reported is shown in *italics* next to the *symbol* 

#### Mixing model

The Margules parameter  $(W_H - TW_S)$  strongly depends on the mixing model (Table 2). While the MM model is consistent with a positive interaction parameter, implying a symmetrical solvus in this binary system, the LCB model requires  $W_G$  to be negative, indicating compound formation and thus the absence of a solvus. Although maintenance of local charge balance (LCB model) may seem appropriate for a mixed-charged coupled substitution [reaction (1)], some facts suggest that the MM model represents titanite solid-solution more accurately. First, the MM model yields a slightly better fit to the data than the LCB model (Table 2). Second, when trying to determine the pressure-dependence of the Margules parameter,  $W_V$ , from the experimental data, application of the MM model resulted in  $W_V = 198 \pm 114 \text{ J mol}^{-1} \text{ kbar}^{-1}$ which is in excellent agreement with  $W_V$  calculated from the excess volume of mixing based on XRD data (Table 2). In contrast, the LCB model did not permit the determination of  $W_V$  at all, but resulted in unreasonably large errors for all refined parameters. The majority of previously reported Margules parameters, determined for other binary solid-solutions, are positive, and only a few cases of negative deviation from ideality are known (Davies and Navrotsky 1981, 1983). Although this should not be used as an argument to dismiss the LCB model as unrealistic, it is nevertheless consistent with our suggestion that the MM model, with positive deviation from ideality, is more appropriate for titanite.

Taylor and Brown (1976) gave a crystal structural explanation as to why the substitution of elements such as  $Al^{3+}$  and  $OH^-$  (and thus  $F^-$ ) need not be spatially coupled in titanite. Titanite has chains of  $TiO_6$ -octahe-

dra with off-centred Ti-atoms, displaced roughly along the polyhedral chain (e.g. Speer and Gibbs 1976). While in ideal  $P2_1/a$ -titanite all Ti-atoms within one chain are shifted in the same direction, the commonly observed anti-phase domains are characterized by opposite displacement of Ti compared with the rest of the chain. Three types of O1-site (bridging site between two TiO<sub>6</sub>octahedra) can be distinguished: (1) within an undisturbed octahedral chain with one Ti displaced towards and one away from the O1-site, (2) at a domain boundary with both Ti displaced away from O1, and (3) at a second type of domain boundary with both Ti displaced toward O1. While type-1 sites are relatively charge balanced, type-2 sites are over-saturated with negative charge, and type-3 sites are under-saturated. Taylor and Brown (1976) pointed out that this charge imbalance could be compensated for by the substitution of F<sup>-</sup> for O<sup>2-</sup> in a type-2 site, and the location of Al<sup>3+</sup> next to a type-3 site, and "emphasised that the substitution of Fe<sup>3+</sup>, Al<sup>3+</sup>, and OH<sup>-</sup> need not be spatially coupled since the structure at a domain boundary could provide the necessary charge balance". Similarly, Hughes et al. (1997) argued that the coupled substitution of Ca<sup>2+</sup> and Ti<sup>4+</sup> by REE<sup>3+</sup> and Al<sup>3+</sup> in titanite does not require the occupation of adjacent sites because the charge imbalance caused by an individual substituent could be compensated by anti-phase domain boundaries. Although charge balance along the domain boundaries is plausible for temperatures below the  $P2_1$ a-A2/a phase transition (T < 825 K, Kek et al. 1997), where Ti is definitely off-centred and domain formation occurs, its applicability to the high temperatures of the experiments of this study (1,073 to 1,273 K) is uncertain. Also, being based on the Ti position, this concept might not explain the distribution of substituents in Al-dominated titanite.

## **Potential solvus**

If the MM model describes the mixing behaviour of titanite correctly, a solvus exists in the system CaTiO-SiO<sub>4</sub>-CaAlFSiO<sub>4</sub>. Although non-ideality is generally temperature-dependent, the narrow temperature range of the piston-cylinder experiments did not permit the determination of the Margules parameter  $W_S$ . Therefore, solvi calculated with the Margules parameters of Table 2, refer to the experimental temperatures of 800 to 1,000 °C (Fig. 7a). In order to investigate whether a solvus could control the composition of natural lower temperature titanites,  $W_S$  has to be estimated. We followed the method described in Pownceby and O'Neill (1994). This estimation is based on the close relation between excess volume and excess entropy (Newton and Wood 1980) by means of its Grüneisen parameter γ. Assuming a Grüneisen parameter similar to that of other solids (compare Poirier 1991, Table 3.3) for CaAlFSiO<sub>4</sub> (between 1 and 1.7), and n=8 (atoms per formula unit) yields excess entropies of mixing

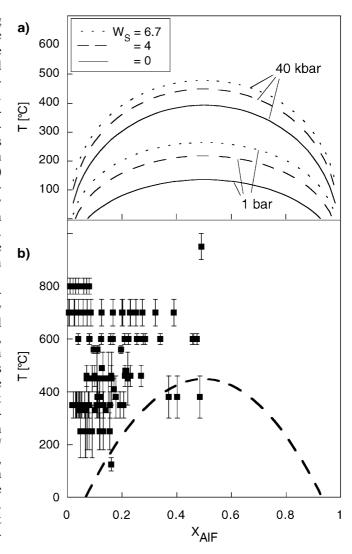


Fig. 7 a Solvi in the binary titanite system as predicted by the MM-model, calculated with different sets of Margules parameters (Table 4), using the equation  $T = W_G(2X-1)/(2Rln[X/1-X])$  (Powell 1978).  $W_S$  in J mol<sup>-1</sup> K<sup>-1</sup>. b Al- and F content of natural and synthetic titanites ( $X_{\rm AIF}$ , atoms per formula unit of component CaAlFSiO<sub>4</sub>) versus their temperature of formation (samples refer to various pressures between 0.5 to 40 kbar). The limited composition would be consistent with a solvus (dashed lines, placed by eye). Data points from (with decreasing temperature): Sobolev and Shatsky (1990), Bernau and Franz (1987), Carswell et al. (1996), Franz and Spear (1985), López Sánchez-Vizcaíno et al. (1997), Enami et al, (1993), Evans and Patrick (1987), Bernau and Franz (1987), Gibert et al. (1990), Yau et al. (1984), Grapes and Watanabe (1992), Makanjuola and Howie (1972), Birch (1983)

**Table 4** Different sets of Margules parameters for titanite  $[Ca(Ti,Al)(O,F)SiO_4]$ , depending on the choice of  $W_S$ 

$\frac{W_H^{\text{a}}}{(\text{kJ mol}^{-1})}$	$W_S$ (J mol <sup>-1</sup> K <sup>-1</sup> )	$W_V$ (J mol <sup>-1</sup> kbar <sup>-1</sup> )
13.6	0.0	214
18.3	4.0	214
21.5	6.7	214

<sup>a</sup>Calculated as  $W_H = 13.6 + 1,173 W_S$ 

between 1 and 1.7 J mol<sup>-1</sup> K<sup>-1</sup>. The corresponding Margules parameters  $W_S$ , calculated with  $S^{\rm exc} = W_S$   $X_{\rm Al}(1-X_{\rm Al})$  (e.g. Wood and Fraser 1978) are 4 and 6.7 J mol<sup>-1</sup> K<sup>-1</sup>. The Margules parameter term ( $W_{H^-}$  T $W_S$ ) of 13.6 kJ mol<sup>-1</sup> refined from the experimental data refers to about 1,173 K (midpoint of the experimental temperature range). For each assumed value of  $W_S$ ,  $W_H$  was calculated with  $W_H$  (J mol<sup>-1</sup>)=13.6+1,173 $W_S$ . The resulting sets of Margules parameters are given in Table 4, and the resulting solvi in Fig. 7a. While the critical temperatures of the solvi with  $W_S$ =0 lie at high P, low T conditions rarely realized on Earth, the temperature-dependent models predict solvi that would mainly affect titanites from the greenshist-, blueshist-and amphibolite-facies (Fig. 7a).

Figure 7b shows a  $T-X_{A1}$  plot of the binary CaTiO-SiO<sub>4</sub>-CaAlFSiO<sub>4</sub> system, based on natural titanite analyses that include fluorine, and for which estimates of the equilibration temperatures of titanite were given. Although the samples refer to different pressures (2 to 40 kbar), the general increase in the maximum  $X_{A1}$  with increasing temperature (up to  $X_{Al} \approx 0.5$ ) is consistent with the presence of a solvus in this system, with a critical temperature between 400 and 600 °C. This temperature range is comparable to the calculated solvi in Fig. 7a. Note, however, that unmixing textures that would imply a solvus, such as an intergrowth of Al-rich and Al-poor titanite, have never been reported from natural samples. Thermodynamic modelling below shows that the solvus is probably truncated or replaced by other reactions, which could explain the absence of titanite with  $X_{A1} > 0.54$ .

#### Thermodynamic modelling

Previous studies of the thermodynamic stability of titanite were exclusively based on CaTiOSiO<sub>4</sub> equilibria. In contrast to this, we investigated the stability of AlFtitanite based on the CaAlFSiO<sub>4</sub> end member, thus exploring parts of compositional space previously unavailable for titanite.

Because the rare occurrence of natural titanite with  $X_{\rm Al} > 0.5$  is yet to be fully understood (Oberti et al. 1991; Troitzsch et al. 1999), the following investigation of phase equilibria in the system CaO-CaF<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>- $SiO_2 \pm TiO_2 \pm H_2O \pm CO_2$  focuses on the maximum possible extent of solid-solution in titanite Ca(Ti, Al)(O,F)SiO<sub>4</sub> in various assemblages. Note that the purpose of this paper is not to present P-T grids readily useable for a large range of natural assemblages because there is limited knowledge of fluorine fugacity in natural rocks. Instead, this work will explore and discuss the basic constraints on Al–F in titanite by choosing simple, F-buffered systems, as a first step towards understanding the more complicated ones, such as found in natural rocks. The stability of CaAlFSiO<sub>4</sub> was modelled for a hypothetical rock (e.g. F-rich calc-silicate), which should represent an ideal medium for the crystallisation of

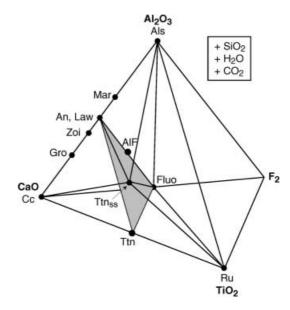


Fig. 8 Tetrahedral phase diagram CaO–Al<sub>2</sub>O<sub>3</sub>–TiO<sub>2</sub>–F<sub>2</sub>, projected from SiO<sub>2</sub>, H<sub>2</sub>O, and CO<sub>2</sub>. *Grey plane* represents the ternary system of the experiments of Troitzsch and Ellis (1999). *Stability lines* are shown for assemblages containing titanite solid solution and fluorite. *Abbreviations* in this and following figures: *AlF* CaAlF-SiO<sub>4</sub>, *Als* aluminosilicate, *An* anorthite, *Cc* calcite, *Fa* fayalite, *Fluo* fluorite, *Gro* grossular, *Ky* kyanite, *Law* lawsonite, *M* magnetite, *Mar* margarite, *Q* quartz, *Ru* rutile, *Ttn* titanite, *Ttn*<sub>ss</sub> titanite solid solution, *Zoi* zoisite, *V* vapour

AlF-rich titanite because it is composed of fluorite, aluminosilicate, quartz and at least one Ca-phase (anorthite, grossular, lawsonite, zoisite, margarite, calcite, depending on fluid species and metamorphic grade), besides titanite solid-solution (Fig. 8).

Note that this investigation focuses on the binary join TiO–AlF, so that the values of  $X_{\rm Al}$  are the amount of aluminium that is substituted with fluorine  $({\rm Ti}^{4+} + {\rm O}^{2-} = {\rm Al}^{3+} + {\rm F}^-)$ . In the hydrous model assemblages considered below, titanite would also contain some water (Hammer et al. 1996), so that the total Al content would be the sum of aluminium coupled with fluorine and water. Ignoring the Al–OH end member here is justified given that the most Al-rich natural titanites, which are to be modelled primarily, only contain up to 10 mol% CaAlOHSiO<sub>4</sub> (e.g. Franz 1987).

#### Fluid-absent equilibria

Figure 9a shows the variation of the Al content of titanite in the fluid-absent system CaO-CaF<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>-SiO<sub>2</sub>, which is well constrained in our experiments. The stability fields of grossular and anorthite are given by

$$\begin{aligned} &Ca_3Al_2Si_3O_{12} + 2Al_2SiO_5 + SiO_2 &= 3 \ CaAl_2Si_2O_8 \\ &Grossular + Kyanite + Quartz = Anorthite \end{aligned} \tag{8}$$

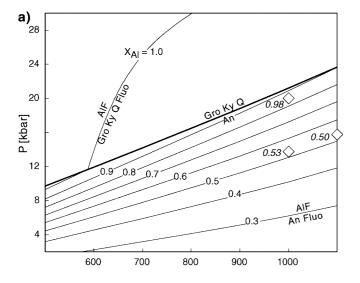
The  $X_{Al}$ -isopleths of titanite coexisting with fluorite and either anorthite, or grossular, kyanite and quartz,

were determined with Eqs. (3) and (4), for the equilibria (2) and

$$\begin{aligned} &6\text{CaAlFSiO}_4 = \text{Ca}_3\text{Al}_2\text{Si}_3\text{O}_{12} + 2\text{Al}_2\text{SiO}_5 + \text{SiO}_2 + 3\text{CaF}_2 \\ &\text{CaAlFSiO}_4 = \text{grossular} + \text{kyanite} + \text{quartz} + \text{fluorite} \end{aligned} \tag{9}$$

Figure 9a predicts that very Al-rich titanite, including the CaAlFSiO<sub>4</sub> end member, should be stable at eclogite facies conditions. The reason why CaAlFSiO<sub>4</sub> has not been reported from natural rocks might be that the complete absence of any fluid is an unrealistic assumption, and that anorthite and grossular usually exist in solid-solution. Reduced anorthite and grossular activities would lower the Al content of titanite at a given pressure and temperature. For example, eclogite facies garnets typically contain less than one-third grossular (Deer et al. 1992). The effect of the garnet composition on Al in titanite in this assemblage is shown in Fig. 9b, which was constructed using the garnet composition from titanite-bearing eclogites of the Tauern Window (32 mol\% grossular, 57 mol\% almandine, 6 mol\% pyrope; Franz and Spear 1985). Thus the dilution of the grossular component to values representative of natural mafic rocks restricts the Al content of titanite to less than about  $X_{A1} = 0.7$  for typical pressures of crustal metamorphism. Large parts of the stability field of titanite with  $X_{\rm Al} > 0.7$  lie beyond the 5 °C km<sup>-1</sup> geotherm, which approximates the limit of pressure and temperature conditions realised on Earth (Schreyer

Fig. 9 a *Thin lines* show the Al-content of titanite [Ca(Ti,Al) (O,F)SiO<sub>4</sub>] coexisting with fluorite and either anorthite (lower P), or grossular, kyanite and quartz (higher P), in the fluid-absent system CaO–CaF<sub>2</sub>–Al<sub>2</sub>O<sub>3</sub>–SiO<sub>2</sub> (reactions 4, 5). *Thick line* is titanite-absent equilibrium (3). *Numbers on isopleths* in this and all following figures refer to  $X_{\rm Al}$  in titanite. *Diamonds* show experimental conditions of Tropper et al. (1999, 2000) of assemblage titanite–anorthite–fluorite ( $\pm$  rutile), with  $X_{\rm Al}$  in *italics*. **b** Same system as **a**, but with garnet Gro<sub>32</sub>Alm<sub>57</sub>Py<sub>6</sub>. *Dashed line* is 5°/km geotherm (Schreyer 1988)

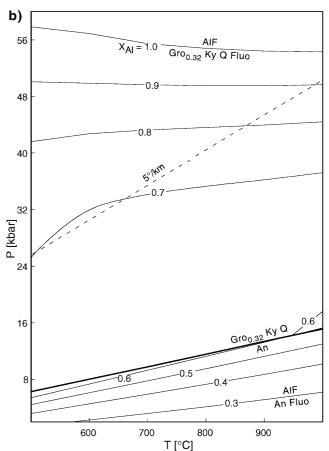


1988). The pure CaAlFSiO<sub>4</sub> end member would only be stable above 55 kbar, well within the 'forbidden zone', which is in agreement with its absence from natural assemblages.

The wide spacing of the isopleths with respect to pressure in the garnet stability field (Fig. 9) is because of the small  $\Delta V$  (0.105 J bar<sup>-1</sup> K<sup>-1</sup>) of reaction (9). This is so small that it changes from positive to negative at about 250 °C, primarily because of the large thermal expansion of fluorite compared with the other product and reactant phases. The sign change of  $\Delta V$  leads to a non-singularity of the isotherms because above this temperature the CaAlFSiO<sub>4</sub> component will be favoured by high pressures whereas, below 250 °C, it will be favoured by low pressures. This non-singularity is the reason for the change in curvature of the isopleths with decreasing temperature (Fig. 9b). If the  $\Delta V$  was assumed constant, and equal to that at standard conditions, the slope of the isopleths in Fig. 9b would be negative, and thus qualitatively incorrect, illustrating the importance of expansion and compressibility in thermodynamic calculations such as these.

#### Fluid-present equilibria: H<sub>2</sub>O

Figure 10a shows a simplified version of the CASH system (e.g. Boettcher 1970; Perkins et al. 1980; Chat-



terjee et al. 1984), with contours of the AlF content of titanite coexisting with fluorite and the various CASH phase assemblages. Several other reactions describing the breakdown of margarite with increasing pressure run subparallel to that shown in Fig. 3a (Chatterjee et al. 1984). These reactions are ignored for the sake of clarity and simplicity. For a similar reason, the breakdown of margarite and quartz to anorthite, kyanite and vapour with increasing temperature (Chatterjee et al. 1984) was omitted. All of these reactions produce relatively small divariant fields, with an insignificant effect on the Al content in titanite. The  $X_{\rm Al}$ -isopleths are based on reaction (2) and reactions

Because of the topology of the P-T grid in Fig. 10a, the maximum  $X_{\rm Al}$  of titanite in this water-saturated system is predominantly controlled by the position of the isopleths in the zoisite stability field. The location of these widely spaced isopleths in P-T space, however, is extremely sensitive to variations in the thermodynamic data used. Errors in the data of any phase in reaction (12) may affect the computed Al content in titanite. For example, by varying the thermodynamic data for CaAlFSiO<sub>4</sub> within given errors (e.g. 2 kJ and 1 J 'assumed error' in enthalpy and entropy, respectively), it is possible to create a scenario by which titanite with  $X_{\rm Al} > 0.55$  is stable only above 24 kbar

$$10\text{CaAlFSiO}_4 + 2\text{H}_2\text{O} = \text{CaAl}_4\text{Si}_2\text{O}_{10}(\text{OH})_2 + 5\text{CaF}_2 + 2\text{Ca}_2\text{Al}_3\text{Si}_3\text{O}_{12}(\text{OH}) + 2\text{SiO}_2$$

$$\text{CaAlFSiO}_4 + \text{H}_2\text{O} = \text{margarite} + \text{fluorite} + \text{zoisite} + \text{quartz}$$

$$2\text{CaAlFSiO}_4 + 2\text{H}_2\text{O} = \text{CaAl}_2\text{Si}_2\text{O}_7(\text{OH})_2\text{H}_2\text{O} + \text{CaF}_2$$

$$\text{CaAlFSiO}_4 + \text{H}_2\text{O} = \text{lawsonite} + \text{fluorite}$$

$$8\text{CaAlFSiO}_4 + \text{H}_2\text{O} = 2\text{Ca}_2\text{Al}_3\text{Si}_3\text{O}_{12}(\text{OH}) + 4\text{CaF}_2 + \text{Al}_2\text{SiO}_5 + \text{SiO}_2$$

$$\text{CaAlFSiO}_4 + \text{H}_2\text{O} = \text{zoisite} + \text{fluorite} + \text{kyanite} + \text{quartz}$$

$$(12)$$

The addition of  $CaF_2$  to the CASH system probably lowers the solidus in Fig. 10 by at least several tens of degrees, as suggested by the eutectic melting temperature of the system  $CaF_2$ – $Ca(OH)_2$  of  $670\pm10$  °C at 1 kbar (Gittins and Tuttle 1964). Two TX-diagrams, derived from Fig. 10a, illustrate the limited extent of solid-solution in titanite at various pressures (Fig. 10b, c).

and 650 °C, which could potentially explain its absence in nature

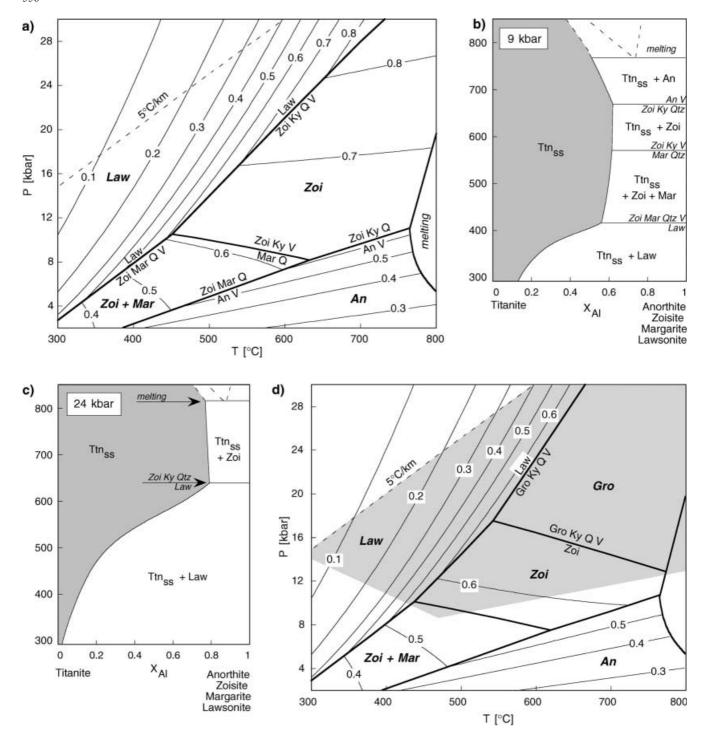
The applicability of Fig. 10a to natural rocks can be significantly improved by considering solid-solution in the Ca–Al phases. Allowing for solid-solution in garnet expands its stability field to lower metamorphic conditions with the reactions (Fig. 10d).

$$\begin{aligned} & 6 \text{Ca}_2 \text{Al}_3 \text{Si}_3 \text{O}_{12} (\text{OH}) = 4 \text{Ca}_3 \text{Al}_2 \text{Si}_3 \text{O}_{12} + 5 \text{Al}_2 \text{Si}_0 + \text{Si}_0 + \text{H}_2 \text{O} \\ & Z \text{oisite} = \text{grossular} + \text{kyanite} + \text{quartz} + \text{H}_2 \text{O} \end{aligned} \tag{13}$$

$$\begin{aligned} & 2 \text{Ca}_2 \text{Al}_2 \text{Si}_3 \text{O}_{12} + 2 \text{Al}_2 \text{O}_{12} + 2 \text{Al}_$$

In the stability fields of lawsonite, anorthite, as well as margarite plus zoisite,  $X_{A1}$  increases towards the zoisite-only stability field (Fig. 10a). The isopleths in the zoisite stability fields are very widely spaced, so that the increase of  $X_{A1}$  with increasing pressure is less in the zoisite than in the anorthite assemblage. Also, the increase of  $X_{A1}$  with increasing temperature in the lawsonite field is slowed down in the zoisite assemblage, and is even reversed at higher pressures (Fig. 10b). Thus the occurrence of very Al-rich titanite is restricted to high metamorphic grades. Titanite with  $X_{A1} > 0.6$ predominantly occurs at eclogite facies conditions, and Al-contents of  $X_{A1} > 0.8$  are restricted to a small wedgeshaped P-T window at very high grade, which might even be limited by melting reactions at higher pressures before the stability of the CaAlFSiO<sub>4</sub> end member is reached.

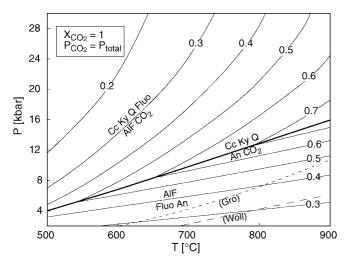
In contrast to grossular, zoisite and lawsonite form less extensive solid-solution. Again, the rocks of the Tauern Window (Franz and Spear 1985) were used as a representative example for an eclogite facies rock with titanite. The activities of the phases were calculated according to the study by Manning and Bohlen (1991)  $(a_{Zoi} = 0.833, grossular activity based on Berman 1990).$ The titanite Al-isopleths in the zoisite stability field move to slightly higher pressures because of the dilution of zoisite. More importantly, the zoisite stability field is cut off by grossular before the  $X_{A1} = 0.7$  isopleth is reached (compare Fig. 10a). Because the isopleths in the grossular stability field are even more widely spaced compared with those in the zoisite field (isopleth  $X_{A1} = 0.7$  lies outside the P-T range shown here), the stability of titanite with  $X_{A1}$ > 0.7 is restricted to significantly higher metamorphic grades compared with the end member calculations.



The topology of Fig. 10d is consistent with the natural occurrence of aluminous titanite, in that titanite with  $X_{\rm Al}$  < 0.6 can be stabilized at pressures and temperatures covering many metamorphic facies, but the most likely occurrence of Al-rich titanite is at eclogite facies conditions. This is consistent with the numerous reports of Al-rich titanite from eclogite terrains (e.g. Smith 1980; Franz and Spear 1985; Krogh et al. 1990; Sobolev and Shatsky 1990; Hirajima et al. 1992; Carswell et al. 1996; Ye and Hirajima 1996), and the less

abundant, yet important finds of Al-rich titanite from lower metamorphic grade (e.g. Boles and Coombs 1977; Franz 1987; Enami et al. 1993; Markl and Paizolo 1999). At temperatures below 450 °C, titanite does not incorporate more than  $X_{\rm AI} = 0.55$  at any pressure. The blueschist facies is especially dominated by lower Al contents, which is in good agreement with natural titanites from such high-pressure, low-temperature terrains typically containing less than  $X_{\rm AI} = 0.20$  (e.g.Makanjuola and Howie 1972; Itaya et al. 1985).

Fig. 10 a Al-content of titanite in the fluid-present system CaO–CaF<sub>2</sub>–Al<sub>2</sub>O<sub>3</sub>–SiO<sub>2</sub>–H<sub>2</sub>O (P<sub>H<sub>2</sub>O</sub> = P<sub>total</sub>). Bold lines: reactions of the CASH-system, with the stability fields of the different Ca–Al phases labelled in bold. Thin lines  $X_{\rm Al}$ -isopleths based on reactions (4) and (6) to (8) in the stability fields An, Mar + Zoi, Law, and Zoi, respectively. Solidus in this and subsequent figures refers to the pure CASH system (Thompson and Ellis 1994). b, c Isobaric T– $X_{\rm Al}$  plots (P<sub>H<sub>2</sub>O</sub> = P<sub>total</sub>) of the pseudo-binary system TiO<sub>2</sub>–AlO<sub>1.5</sub>, based on a, illustrating the limited extent of solid-solution of titanite in various assemblages with fluorite. Phase compositions in the melting region are semi-quantitative estimates. d Effect of solid-solution in grossular and zoisite on calculated reactions in the CASH system and titanite  $X_{\rm Al}$  isopleths (a) ( $X_{\rm Gro}$  = 0.32, a<sub>Zoi</sub> = 0.833). Eclogite facies shaded



**Fig. 11** Al-content of titanite, coexisting with a pure  $CO_2$ -fluid in the system CaO– $CaF_2$ – $Al_2O_3$ – $SiO_2$ – $CO_2$ . Grossular is absent, as the reaction calcite + kyanite + quartz = grossular +  $CO_2$  (*Gro*) is metastable. Also shown is reaction calcite + kyanite = wollastonite +  $CO_2$  (*Woll*). Melting at or below  $880 \pm 10$  °C (eutectic temperature in the binary system  $CaF_2$ – $CaCO_3$  at 1 kbar, Gittins and Tuttle 1964)

The Al and F contents of titanite in the Tauern Window rocks span a large range, with a maximum value of  $X_{AlF} = 0.54$  in one fluorite- and zoisite-bearing rock (sample 79-102, Franz and Spear 1985). The peak metamorphic conditions of these rocks, at which the Al-rich titanite is thought to have equilibrated, are 20 ± 2 kbar, 600 °C, with an almost pure H<sub>2</sub>O-fluid (Franz and Spear 1983). At these conditions, however, Fig. 10d predicts Al contents of about  $X_{Al} = 0.65$ . This inconsistency could be because not all phases of the buffer assemblage are present in this sample (quartz and kyanite were not mentioned by Franz and Spear 1985). More likely, it could simply be because of the large uncertainties attached to the isopleth position, which can be estimated to be of the order of  $X_{A1} \pm 0.25$  for the zoisite stability field. This uncertainty is enormous in petrological terms, and rules out the confident use of titanite as a geothermobarometer in this assemblage.

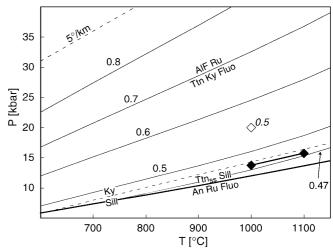


Fig. 12 Al-content in titanite, coexisting with rutile, kyanite and fluorite [reaction (15)]. Bold line is reaction (16) referring to  $X_{\rm Al} = 0.45 \pm 0.03$ . Open diamond shows experimental conditions of Tropper et al. (1999) of assemblage titanite–fluorite–kyanite–rutile, with  $X_{\rm Al}$  given in italics. Black diamonds represent stability limit of the assemblage anorthite–rutile–titanite–fluorite in experiments by Tropper et al. (2000;  $X_{\rm Al}$  as in Fig. 9a)

### Fluid-present equilibria: CO<sub>2</sub>

High grade metamorphic fluids such as in granulites are typically CO<sub>2</sub>-rich. Figure 11 shows the AlF content of titanite in equilibrium with CAS-CO<sub>2</sub> phases, described by the reactions

$$\begin{aligned} &CaCO_3 + Al_2SiO_5 + SiO_2 &= CaAl_2Si_2O_8 + CO_2 \\ &Calcite + kyanite + quartz = anorthite &+ CO_2 \end{aligned} \tag{15}$$

$$CaCO_3+Al_2SiO_5+SiO_2 + CaF_2 = 2CaAlFSiO_4+CO_2$$
  
 $Calcite + kyanite + quartz + fluorite = CaAlFSiO_4 + CO_2$  (16)

Figure 11 demonstrates that  $P_{CO_2} = P_{total}$  restricts the Al content of titanite, yet again, to less than about  $X_{\rm Al} = 0.75$ , at crustal conditions. Although at higher pressure the isopleths of the decarbonation reaction (16) swing back to lower temperatures, titanite with  $X_{\rm Al} > 0.7$  becomes stable again only at extremely high pressures (for example, 55 kbar at 750 °C), possibly not realised in natural rocks.

#### Equilibria with TiO<sub>2</sub>

A simple fluid-absent reaction relating the two titanite end members is (Fig. 12)

$$\begin{aligned} 2 CaAlFSiO_4 + TiO_2 &= CaTiOSiO_4 + &Al_2SiO_5 &+ CaF_2 \\ CaAlFSiO_4 + rutile &= titanite &+ aluminosilicate + fluorite \end{aligned} \tag{17}$$

Again, natural titanite with extremely high Al contents and the CaAlFSiO<sub>4</sub> end member are not to be expected in this assemblage because their isopleths lie beyond the 5 °C-km<sup>-1</sup> geotherm. The assemblage titanite–rutile–

aluminosilicate–fluorite [equilibrium (17)] is limited towards lower pressure by the breakdown of titanite  $(X_{\rm Al} = 0.45 \pm 0.03)$  and sillimanite by the reaction

$$\begin{split} &[(1-n)\text{CaTiOSiO}_5 + n\text{CaAlFSiO}_4] + (1-n)\text{Al}_2\text{SiO}_5 \\ &= (1-n/2)\text{CaAl}_2\text{Si}_2\text{O}_8 + (n/2)\text{CaF}_2 + (1-n)\text{TiO}_2 \\ &\text{Titanite}_{\text{SS}} + \text{Sillimanite} \\ &= \text{Anorthite} + \text{Fluorite} + \text{Rutile} \end{split} \tag{18}$$

where  $n = X_{Al}$ . This equilibrium is simply the summation of the two reactions limiting the stability of each end member, i.e. reaction (2) and

$$CaTiOSiO_4 + Al_2SiO_5 = CaAl_2Si_2O_8 + TiO_2$$

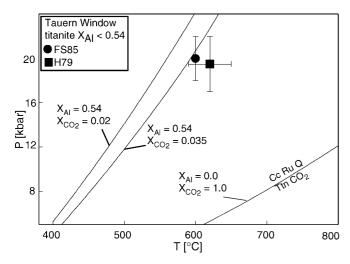
$$Titanite + aluminosilicate = anorthite + rutile$$
(19)

The displacement of this reaction in the presence of fluorite, which allows for titanite solid-solution along the binary join TiO–AIF discussed here, was investigated recently with piston-cylinder experiments by Tropper et al. (1999, 2000). They reported titanite with  $X_{\rm AI} = 0.50$  from the synthetic assemblage titanite–rutile–kyanite–fluorite at 20 kbar and 1,000 °C (open diamond, Fig. 12), which agrees well with the predicted  $X_{\rm AI} = 0.55$  isopleth of equilibrium (17). Tropper et al. (2000) determined the stability limit of the assemblage anorthite–rutile–titanite–fluorite (black diamonds, Fig. 12), which differs less than  $2 \pm 0.2$  kbar from that calculated here with reaction (17).

The stability of titanite in calcareous rocks can be described by the reaction

$$CaCO_3+$$
  $SiO_2$   $+TiO_2 = CaTiOSiO_4 + CO_2$   
 $Calcite + quartz/coesite + rutile = titanite + CO_2$  (20)

This equilibrium restricts titanite in the presence of a pure CO<sub>2</sub> fluid to low pressures and high temperatures



**Fig. 13** Dependence of reaction (18) on  $X_{\rm Al}$  of titanite and the  $X_{\rm CO_2}$  of the coexisting fluid ( $P_{\rm fluid} = P_{\rm total}$ ). *Data points* represent peak-metamorphic conditions for titanite-bearing eclogites from the Tauern Window. Estimates of fluid composition are  $X_{\rm CO_2} = 0.02$  (Holland 1979) and  $X_{\rm CO_2} = 0.035$  (Franz and Spear 1983). *FS85* Franz and Spear 1985; *H79* Holland 1979. Calcite–aragonite transition not shown

(Fig. 9; Hunt and Kerrick 1977; Jacobs and Kerrick 1981). As pointed out previously (Carswell et al. 1996; Frost et al. 2001) the stability of titanite can be extended to higher pressures by diluting the CO<sub>2</sub> content of the fluid, as well as by diluting the titanite component in solid-solution. This explains the presence of Al-rich titanite in calcareous eclogite-facies rocks, such as the carbonate-bearing eclogites from Dabieshan (Carswell et al. 1996), siliceous dolomites in eclogite facies rocks of the Tauern Window (Franz and Spear 1985), and the calc-silicates and marbles in the eclogite complex at Tromsø (Krogh et al. 1990). This effect is demonstrated in Fig. 13 with the rocks from the Tauern Window, which equilibrated at eclogite-facies conditions in the presence of an almost pure H<sub>2</sub>O-fluid (Holland 1979; Franz and Spear 1983, 1985). The dilution of both the titanite component with CaAlFSiO<sub>4</sub> (maximum  $X_{Al} = 0.54$ , Franz and Spear 1985), and the CO<sub>2</sub> fluid with H<sub>2</sub>O, shifts the reaction to pressures just high enough to stabilise titanite at the given metamorphic conditions.

#### Fluorine fugacity

Previous studies showed that the titanite composition depends on the fugacities of oxygen and fluorine (Markl and Piazolo 1999). For example, Bohlen and Essene (1978) investigated fluorine-rich assemblages from several locations in the Adirondacks, USA, and the buffering effect on fluorine and oxygen fugacities. According to their calculations, the stability of titanite is restricted to low fluorine fugacities with the reaction (Fig. 14)

$$\begin{aligned} &2CaTiOSiO_4 + 2F_2 = 2CaF_2 + 2TiO_2 + 2SiO_2 + O_2 \\ &Titanite \quad + F_2 = fluorite + rutile + quartz + O_2 \end{aligned} \tag{21}$$

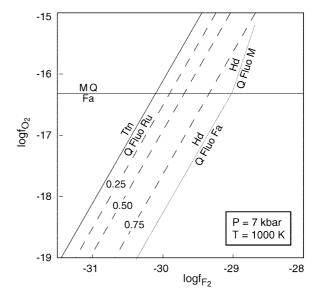
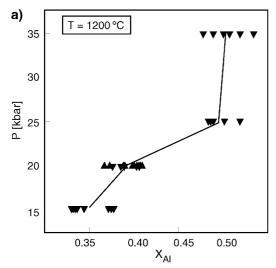
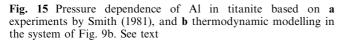


Fig. 14 Bold lines are reactions (21) and (22) calculated using thermodynamic data given in Bohlen and Essene (1978). Dashed lines are titanite  $X_{Al}$ -isopleths

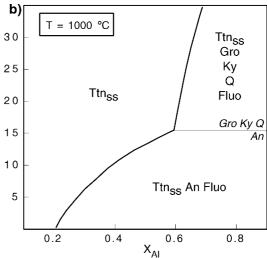




whereas the assemblage hedenbergite–quartz–fluorite–fayalite is restricted to higher  $f_{F_2}$  with reaction

$$\begin{aligned} 2 Ca Fe Si_2 O_6 & + 2 F_2 &= 2 Ca F_2 & + Fe_2 Si O_4 + & 3 Si O_2 + O_2 \\ Hedenbergite &+ F_2 &= fluorite + fayalite + quartz + O_2 \end{aligned} \tag{22}$$

In agreement with this, Bohlen and Essene (1978) found the assemblage hedenbergite-quartz-fluoritefayalite without titanite in the Wanakena fayalitegranite. However, they noted that Leonard and Buddington (1964) reported titanite in the same rock. This would pose a problem if the titanite was in equilibrium with the assemblage described by Bohlen and Essene (1978). They suggested that either uncertainties in the thermodynamic data, particularly those of titanite, could account for this possible inconsistency, or that the titanite contains additional components, which extend its stability field to higher fluorine fugacities. Although analyses of this titanite were not reported, the high fluorine content of the rocks suggests that the titanite may contain Al and F, which could extend its stability field. Figure 14 shows the shift of reaction (22) with increasing CaAlFSiO<sub>4</sub> content of titanite. Even Al contents as high as  $X_{Al} = 0.75$ , which exceeds all values previously reported from natural rocks, cannot extend the stability of titanite sufficiently to overlap with the assemblage hedenbergite-quartzfluorite-fayalite. Note that reaction (22) is calculated for the end member phases. If phase compositions of the Wanakena granite were considered, this equilibrium would plot at slightly higher fluorine fugacities, thus even further away from the titanite stability field (Bohlen and Essene 1978). Because Al in titanite cannot reconcile the calculations with the observations, it can be concluded that the inconsistency between the calculated petrogenetic grid by Bohlen and Essene (1978) and the observed mineral assemblage, must be



caused by errors in the thermodynamic data they used. If the same reactions are calculated with the data from Robie and Hemingway (1995), the titanite stability field overlaps with the hedenbergite–quartz–fluorite–fayalite assemblage, and the problem reported by Bohlen and Essene (1978) is resolved.

#### **Summary and conclusions**

The CaTiOSiO<sub>4</sub>–CaAlFSiO<sub>4</sub> activity–composition relations and mixing models provide important information for future thermodynamic studies of titanite as a petrogenetic indicator. The effect of the fluorine fugacity on the Al content of titanite can now be quantified via the end member CaAlFSiO<sub>4</sub>. Future work on the waterbearing end member (CaAlOHSiO<sub>4</sub>) is highly desirable in order to extend the application of Al–titanite equilibria to a wider range of natural rocks.

The calculated P-T grids agree with natural occurrences of Al-bearing titanite in many aspects. Titanite solid-solution with up to  $X_{\rm Al} = 0.6$  can occur in most metamorphic facies, but more Al-rich titanites are generally restricted to eclogite facies conditions. Titanite with  $X_{A1} > 0.8$ , and the pure CaAlFSiO<sub>4</sub> end member can only be stable at pressures and temperatures accessible to crustal metamorphism in the absence of any fluid, be it H<sub>2</sub>O or CO<sub>2</sub>, and if the coexisting garnet is pure grossular. These conditions, however, might never be realised in nature. In more realistic scenarios accounting for garnet solid-solution and/or the presence of a fluid, titanite with  $X_{A1} > 0.75$  does not occur, either because it is restricted to extremely high pressures rarely realised in natural rocks (Figs. 9b and 11) or because it is unstable with respect to other phases or melt (Fig. 10b). While the presence of H<sub>2</sub>O destabilises high concentrations of CaAlFSiO<sub>4</sub> with respect to zoisite or grossular (Fig. 10d), a CO<sub>2</sub>-bearing fluid promotes its breakdown to an assemblage with calcite (Fig. 11). This confirms the hypothesis of Troitzsch and Ellis (1999) that very Al-rich titanite and CaAlFSiO<sub>4</sub> are only stable in simple chemical systems such as in experiments, and reconciles the apparent contradiction between the synthesis of CaAlFSiO<sub>4</sub>, and its absence from natural rocks. The calculated P–T grids also suggest that the blueschist facies is dominated by titanite of lower Al content, which is in good agreement with natural observations.

The last point illustrates that the simple relationship between pressure, temperature and titanite composition, as observed in our experiments and those of Smith (1981; i.e. increasing pressure and decreasing temperature promote Al in titanite), cannot be used as a 'rule of thumb', but depends on the buffering effect of the specific mineral assemblage. The Al content of titanite equilibrated with lawsonite and fluorite, for example, behaves inversely because of the large volume contribution of the fluid phase (Fig. 10a).

Reactions such as Eq. (20) seem to be good indicators for pressure-temperature-fluid composition relationships (Fig. 13). In contrast, the extremely widely spaced  $X_{Al}$ -isopleths in high-pressure assemblages with zoisite and grossular are very sensitive to changes or errors in the input data. Thus, the uncertainties attached to the Al content computed with these equilibria are very large and do not allow the use of Al in titanite as a reliable geothermobarometer. Such widely spaced isopleths may in fact be responsible for the 'levelling out' of the Al contents in titanite at about  $X_{\rm Al} = 0.53$  between 25 and 35 kbar in the experiments by Smith (1981). This is suggested by the striking similarity between the  $P-X_{A1}$  plot by Smith (1981), and that, for example, based on Fig. 9b of this study (Fig. 15). According to Smith (1981) various phase assemblages occur in his experiments (titanite-rutilecorundum-melt with either kyanite, quartz or fluorite), thus allowing for a possible reaction between 20 and 25 kbar to explain the change in slope (Fig. 15a). Unfortunately, this system cannot be modelled in detail because the assemblages for individual experiments were not given by Smith (1981). Moreover, the presence of melt prevents straightforward thermodynamic modelling.

The multi-site mixing model of titanite used throughout the present study implies the existence of a solvus in the binary TiO-AlF titanite system. This seems to be contradicted by the lack of reports of natural titanite unmixing into Al-rich and Al-poor domains, but may be explained, for example, with Fig. 10b, c. Here the solvus would lie in the Ttn<sub>SS</sub> + Law field. Although the curved shape of the  $Ttn_{SS}$  + Law stability field at low Al contents suggests that the solvus is approached, it is not reached because very Al-rich titanite is not stable in this wet system. The stability field of Ttnss (shaded in Fig. 10) is cut off at high Al contents by reactions stabilising other Ca–Al phases and fluorite. Because of the instability of very Al-rich titanite in most systems, the situation in Fig. 10b, c may be typical for Al-titanite in general. Instead of unmixing into two titanite phases, the breakdown of Al-rich titanite to a vermicular intergrowth of Al-poor titanite and anorthite can be observed in rocks (Carswell et al. 1996).

The instability of the CaAlFSiO<sub>4</sub> end member with respect to other phases in almost all assemblages investigated here is in very good agreement with the crystal structure data of Troitzsch and Ellis (1999) and Troitzsch et al. (1999), which indicate that the titanite structure is not well suited to accommodate Al and F instead of Ti and O. High bond valence sums at the Ca and O1-site, and polyhedral distortion, indicate structural stresses, lattice energies of small magnitudes, and thus low thermodynamic stability of CaAlFSiO<sub>4</sub> (i.e. high Gibbs free energy), manifested in its standard state properties. The limiting value of  $X_{A1} = 0.65 \pm 0.15$ observed in the P-T grids presented here supports the hypothesis based on crystal structure data that titanite stability decreases when  $X_{A1}$  exceeds 0.6 significantly (Troitzsch et al. 1999). Note, however, that the activity– composition relations are simple, without any significant anomaly at high Al contents, which could be the thermodynamic expression of the crystal structural problems setting in at about  $X_{\rm Al} = 0.65$ . Thus, the limiting composition of titanite in the petrogenetic grids cannot be linked directly to the crystal structural problems observed at these Al contents via the activity of titanite. There does not seem to be a particular 'catastrophic' crystal structural process, such as the collapse of the octahedral bonds at  $X_{Al} = 0.40$  (Troitzsch et al. 1999), which could act as an energy barrier, preventing high Al-titanite formation, as this would show in the activity-composition relations. Rather, it seems to be continuous crystal structural changes that affect the thermodynamic stability of titanite, such as the smooth change in bond valence sums from one end member to the other (Troitzsch et al. 1999), which might not stand out as anomalies in activity-composition relationships.

Thus, the structural problems at  $X_{\rm Al} > 0.60$ , and the limiting composition in the petrogenetic grids have the same cause, i.e. the incorporation of an increasing amount of an end member with a less suited structure and thus lower thermodynamic stability. The maximum Al content of natural titanites of  $X_{\rm Al} \approx 0.54$ , is probably simply marking the point beyond which the thermodynamically less favourable CaAlFSiO<sub>4</sub> starts to dominate over CaTiOSiO<sub>4</sub> in the solid-solution.

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#### **Appendix**

#### Table A1

Coefficients of curve fit polynomials representing the unit-cell dimensions a, b and c, as used for the indirect

determination of the composition of fine-grained, synthetic titanite. The polynomials are defined as

$$Y_{a,b,c,\beta,V,BVS} = \sum (M_n)_{a,b,c,\beta,V,BVS} X^n$$
 with  $n = 0, 1, \ldots, 5$ .

whereby X represents the independent variable  $X_{Al}$ , Y is the dependent variable a, b, or c, and  $M_n$  are the polynomial coefficients.

Unit cell dimension	a [Å]	a [Å]	b [Å]	c [Å]
$X_{A1}$ range $M_0$ $M_1$ $M_2$ $M_3$ $M_4$ $M_5$	0.00-0.18 7.0612 -0.4906 9.8272 -84.343 322.67 460.46	0.18–1.00 7.0477 0.0675 -0.2876 0.0886	0.00-1.00 8.7135 -0.3005 0.6571 -1.6357 1.727 -0.6529	0.00-1.00 6.5583 -0.2159 0.6507 -1.5301 1.5398 -0.5628

#### Table A2

Enthalpy of formation from the elements  $(d_f H^0)$  and the standard state entropy  $(S^0)$  of CaAlFSiO<sub>4</sub>, and Margules parameter at experimental temperature  $(W_H - TW_S)$ , determined with various thermodynamic data for anorthite (Anor) and fluorite (Fluo). Data bases: Robie and Hemingway (1995; RH), two updates of the program SUPCRT (Johnson et al. 1991; SUP94 and SUP98), Holland and Powell (1998; HP). The calculation of the Gibbs energy of formation  $(d_f H^0)$  was based on the data for the elements by Robie and Hemingway (1995). The standard state is 298.15 K and 1 bar.

Data Anor	Data Fluo	MM-model	LCB-model
RH HP SUP94 SUP98	RH RH SUP94 SUP98	$d_f H^0$ (kJ mol <sup>-1</sup> ) -2,743.7 ± 3.0 -2,744.3 ± 2.0 -2,741.1 ± 3.0 -2,734.0 ± 3.0	$d_f H^0$ (kJ mol <sup>-1</sup> ) -2,736.7 ± 3.1 -2,737.3 ± 2.1 -2,734.1 ± 3.1 -2,727.0 ± 3.1
RH HP SUP	RH RH SUP	$S^0$ (J mol <sup>-1</sup> K <sup>-1</sup> ) 104.2 ± 1.1 103.7 ± 1.1 108.2 ± 1.1	$S^{0}$ (kJ mol <sup>-1</sup> K <sup>-1</sup> ) 110.6 ± 1.2 110.2 ± 1.2 114.7 ± 1.2
RH HP SUP	RH RH SUP	$W_H$ -T $W_S$ (J mol <sup>-1</sup> ) 13.6 ± 0.4 13.6 ± 0.4 13.6 ± 0.4	$W_H$ -T $W_S$ (J mol <sup>-1</sup> ) -9.1 ± 0.4 -9.1 ± 0.4 -9.1 ± 0.4
RH HP SUP94 SUP98	RH RH SUP94 SUP98	$d_f G^0$ (kJ mol <sup>-1</sup> ) -2,595.4 ± 2.8 -2,595.8 ± 1.8 -2,594.3 ± 3.0 -2,587.0 ± 3.0	$d_jG^0$ (kJ mol <sup>-1</sup> ) -2,590.3 ± 2.8 -2,590.8 ± 1.8 -2,589.3 ± 3.0 -2,581.9 ± 3.0

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