

An experimental study of anorthosite dissolution in lunar picritic magmas: Implications for crustal assimilation processes

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Abstract

Experiments characterizing the kinetics of anorthosite dissolution in lunar picritic magmas (very low-Ti, low-Ti, and high-Ti picritic glasses) were conducted at 0.6 GPa and 1250–1400 °C using the dissolution couple method. Reaction between the anorthosite and lunar picritic magmas at 1250–1300 °C produced a spinel + melt layer. Reaction between the anorthosite and an olivine-saturated low-Ti magma at 1250–1300 °C produced a crystal-free region between the spinel + melt layer and the olivine-saturated magma. The anorthosite dissolution experiments conducted at 1400 °C simply dissolved anorthosite and did not result in a crystal-bearing region. The rate of anorthosite dissolution strongly depends on temperature and composition of the reacting melt. Concentration profiles that develop during anorthosite dissolution are nonlinear and extend from the picritic glass compositions to anorthite. These profiles feature a large and continuous variation in melt density and viscosity from the anorthosite-melt interface to the initial picritic magmas. In both the low-Ti and high-Ti magmas the diffusive fluxes of TiO₂, Al₂O₃, and SiO₂ are strongly coupled to the concentration gradients of CaO and FeO. Anorthosite dissolution may play an important role in producing the chemical variability of the lunar picritic magmas, the origin of spinel in the lunar basalts and picritic glasses, and the petrogenesis of the high-Al basalts.

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1. Introduction

Ferroan anorthosites (FANs) are a major component of the ancient lunar crust. According to the giant impact theory, lunar anorthosite crust was formed via plagioclase flotation in a globally distributed lunar magma ocean (e.g., Warren, 1985; Papike et al., 1998; Shearer and Papike, 1999 and references therein). The Mg-suite and alkali-suite plutonic rocks are samples from generally younger crustal intrusions. Plagioclase in FANs has a high anorthite content (An₉₄–An₉₉, typical modal abundance > 90%). Mafic minerals in FANs are predominately low-Ca pyroxenes (Mg# ~40–74) plus (typically) smaller amounts of olivine and traces of ilmenite, chromite, and Fe–Ni metal (e.g., Papike et al., 1998 and references therein). Whole rock and

mineral compositions suggest that FANs crystallized from parent magmas after 75–80% crystallization of the lunar magma ocean (e.g., Snyder et al., 1992).

The younger ages of the lunar volcanic rocks relative to the anorthite-rich crust suggests that the mare basalts and picritic glasses may have interacted with plagioclase-rich lithologies before eruption on the surface. The nature of the interaction varies from assimilation and crystallization along the walls of magma conduit in the lunar crust to assimilation occurring in magma chambers within or at the base of the lunar crust. The extent of interaction between lunar magmas and anorthite-rich crust is a fundamentally important question in understanding the evolution of lunar magmas as well as the inferred properties of the mantle source regions.

Both thermal and chemical interactions between the magma and anorthosite crust are likely to play an important role in lunar picritic magma differentiation. Thermal interactions, driven by latent heat and differences in temperature between the magma and wallrock, result in

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melting of the anorthite-rich wallrock and local crystallization of the picritic magma. Chemical interactions, driven by difference in composition or chemical potential between the melt and wallrock, result in anorthite-rich wallrock dissolution. To date, the most detailed study of anorthosite dissolution was conducted by Finnila et al. (1994) in a high-Ti picritic magma. Finnila et al. (1994) concluded that modification of the high-Ti picritic magmas by anorthosite assimilation is unlikely because the thermal constraints of melting and assimilation are too restrictive, and that the rates of anorthosite dissolution are too slow to allow significant modification of the magma compositions.

Coupling the thermal and the chemical constraints on anorthosite assimilation opens up some new possibilities not addressed by Finnila et al. (1994). Fig. 1 shows the forsterite–anorthite (Fo–An) phase diagram (after Morse, 1994) and a hypothetical cross section through a magma filled dike within the lunar crust. The physical mechanisms explored by Finnila et al. (1994) include melting of the anorthite-rich crust by intruding hot picritic magma coupled with mixing of the resulting melt with the intruding melt. Finnila et al. (1994) argues that the energetics of the interactions between the hot picritic magma and the cold anorthite-rich crust will limit the amount of assimilation. However, the thermal constraints can be relaxed with observations of the Fo–An phase diagram and assumptions about the model systems. We envision a case where a hot olivine-saturated picritic magma intrudes a cooler anorthosite body (Fig. 1b). The most important aspect of this process is that anorthosite assimilation will not necessarily result in significant olivine crystallization. Anorthosite assimilation into an olivine-saturated magma may lower the liquidus of the magma mixture (Fig. 1a). As a hot olivine-saturated picritic magma dissolves the cooler anorthosite the temperature of the magma will decrease because of the energy required to dissolve anorthite. However, the change in magma chemistry resulting from anorthosite dissolution will lower the liquidus temperature of the magma. The exact behavior of the system will depend on the balance of energy lost due to anorthosite assimilation relative to the reduction of the liquidus temperature. It is possible that anorthosite assimilation will result in a local reduction in the crystallinity of the reacting melt, and potentially brings part of the system above the liquidus (thick dashed curve, Fig. 1a). Physically this may mean that a crystal-free or spinel saturated reactive boundary layer develops between the olivine-saturated magma and the anorthosite host rock. Additionally, if we assume the volume of melt flowing through a dike in the crust is large, then it seems reasonable that the heat of the incoming magma will buffer the temperature of the wallrock preventing extensive cooling of the magma during assimilation. Other physical properties of the reacting magma such as density and viscosity will also be significantly modified by anorthosite assimilation.

In this paper, we present results from an experimental study of anorthosite dissolution in lunar picritic magmas

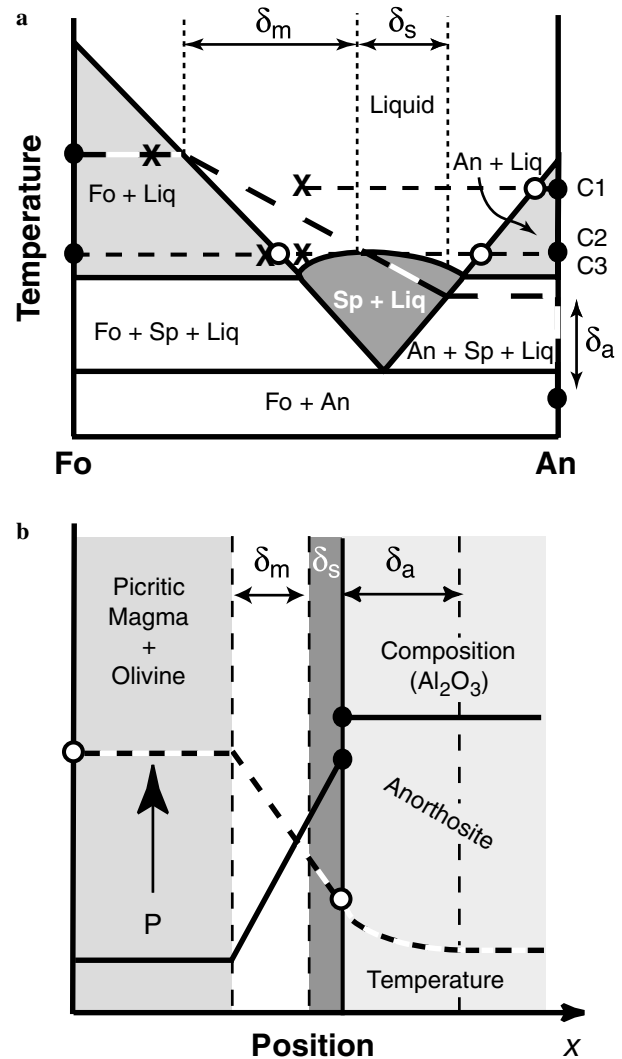


Fig. 1. (a) Cartoon of the forsterite–anorthite binary phase diagram (after Morse, 1994). Dashed lines in (a) correspond to either our experimental conditions (the thin dashed horizontal lines, C1–C3) or a hypothetical temperature–chemical distribution associated with olivine-saturated magma flowing in a dike through the anorthosite crust (thick dashed curve). The filled circles are the solid compositions, open circles are the liquidus composition and the Xs are the bulk composition of the reacting magma. In case 1 (C1), anorthosite dissolution was conducted at high temperatures so that the magma away from the anorthosite is crystal-free (1400 °C). In case 2 (C2), dissolution was conducted at temperatures low enough to stabilize spinel near the interface with the anorthosite (1250–1300 °C). In case 3 (C3), anorthosite dissolved into an olivine-saturated picritic magma, resulting in a spinel layer and a crystal-free region (1250–1300 °C). (b) A cross section through a hypothetical dike in the anorthosite crust. The left is the hotter olivine-saturated picritic magma, and the right is the cooler anorthosite crust. Separating the olivine-saturated magma from the anorthosite wallrock is a crystal-free region (δ_m) and the spinel + liquid region (δ_s). δ_a is the thermal boundary layer within the anorthosite. The thick dashed curve (temperature) and the thick solid curve (Al_2O_3 concentration) are a suggested thermal–chemical path that may result when a high temperature olivine-saturated magma reacts with a cooler anorthosite crust.

with the purpose of exploring the possible interactions between picritic mare basalts and the lunar anorthosite crust. We explore the chemical and physical consequences of

Table 1
Starting compositions

Oxide	Very low-Ti ^a (A15 Green Glass)	Low-Ti ^b (A15 Yellow Glass)	High-Ti ^c (A15 Red Glass)
SiO ₂	48.29	44.26	36.76
TiO ₂	0.23	3.63	13.89
Al ₂ O ₃	7.77	9.08	7.51
Cr ₂ O ₃	0.55	0.53	0.76
FeO ^d	16.12	21.65	22.95
MnO	0.19	0.57	0.05
MgO	18.26	10.97	10.16
CaO	8.59	8.76	8.57
Na ₂ O	0.00	0.37	0.59
Total	100.00	99.82	101.24
Mg#	66.88	47.46	44.11

^a A15C (in wt%), Elkins-Tanton et al. (2003).

^b A15YG-2C, Shearer and Papike (1993).

^c Delano (1980).

^d Total FeO.

anorthosite dissolution over a range of temperatures and in three different picritic magma compositions (Table 1). We then compare the chemical variations observed in the lunar picritic glasses and high-Al basalts with our experimental results and explore the extent of anorthosite assimilation in the petrogenesis of these mafic and ultramafic magmas.

2. Experimental methods

Experiments characterizing anorthosite reactive dissolution in lunar picritic magmas were carried out at 1250–1400 °C and 0.6 GPa using a 19.1 mm piston–cylinder apparatus following the method of Morgan and Liang (2003, 2005). We acknowledge that the minimum pressures accessible by piston cylinder are deeper than the lunar crust. However, the differences in phase equilibria between our experimental pressure and that of the lunar crust is minor with shifts in the anorthite and spinel phase boundaries. We feel the use of the proven dissolution method far outweighed the minor differences in phase equilibria resulting from the differences in pressure.

2.1. Sample preparation

The starting materials for the melts are a very low-Ti (VLT) Apollo 15 green glass (Elkins-Tanton et al., 2003), a low-Ti Apollo 15 yellow glass (Shearer and Papike, 1993), and a high-Ti Apollo 15 red glass (Delano, 1980), each synthesized from high purity oxides and carbonates (Table 1). In addition, an olivine-saturated low-Ti melt was made by adding 10wt% fine grained, optical clean olivine from Kilbourne Hole, NM (Mg# = 91, composition given in Table 1 of Morgan and Liang, 2005) to the low-Ti glass. The powders were carefully weighed and mixed together under ethanol in an agate mortar and pestle. Each powder was then run at 900 °C at the iron-wüstite (IW)

buffer in a mixed gas furnace for 1 h. The reduced and decarbonated powders were then reground under ethanol in the agate mortar and pestle for 20 min and stored in a 110 °C vacuum oven for at least 24 h. The anorthosite was created by crystallizing synthetic An100 glass powder at the same conditions as those of the dissolution experiments described below.

2.2. Procedures

The furnace assembly consists of a molybdenum capsule sandwiched between two crushable MgO spacers in a graphite, Pyrex[®], and salt sleeve. The molybdenum capsule (6.5 mm OD and 10 mm long) was lined with a platinum tube (4 mm OD, 3.8 mm ID) and a graphite inner sleeve (3.8 mm OD, 2 mm ID). Use of the graphite- and platinum-lined molybdenum (C–Pt–Mo) capsule eliminates sample-container reactions and assures reasonably good geometry of the dissolution couple (Fig. 2).

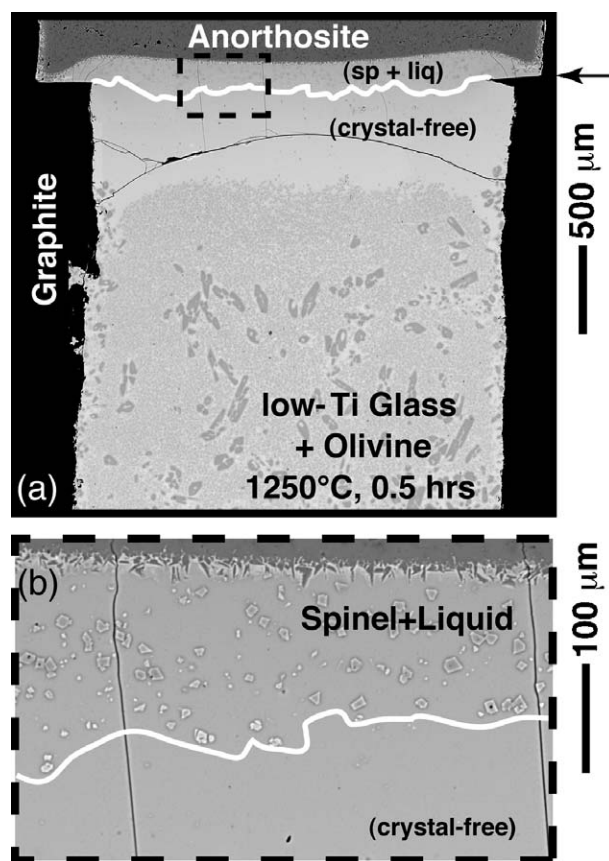


Fig. 2. BSE images of the anorthosite dissolution into an olivine-saturated low-Ti picritic magma (Andis13, 1250 °C, 0.6 GPa, 0.5 h). (a) Low magnification BSE image showing the capsule geometry, with anorthosite (top), the spinel + liquid region (sp + liq), the crystal-free region (crystal-free), and the olivine-saturated low-Ti glass. (b) Higher magnification BSE image of the spinel + liquid region. The white lines drawn on the images mark the bottom boundary of the spinel + liquid region. The arrow marks the original interface between the anorthosite and the olivine-saturated picritic magma.

Table 2
Summary of anorthosite dissolution experiments

Run #	T (°C)	Pressure (GPa)	Duration ^a (h)	Dissolution distance ^b (μm)
<i>Very low-Ti (A15 Green Glass)</i>				
Andis1	1420	0.8	8.0 (21)	949 ± 33
Andis2	1400	0.6	1.0 (8)	466 ± 11
Andis3	1400	0.6	0.3 (21)	254 ± 9
<i>Low-Ti (A15 Yellow Glass)</i>				
Andis4	1400	0.6	0.3 (24)	316 ± 5
Andis6	1400	0.6	1.0 (8)	518 ± 5
Andis8	1400	0.6	0.1 (8)	184 ± 7
Andis10	1300	0.6	0.5 (8)	191 ± 4
Andis11	1250	0.6	1.0 (12)	154 ± 6
<i>High-Ti (A15 Red Glass)</i>				
Andis5	1400	0.6	0.3 (24)	369 ± 5
Andis7	1400	0.6	1.0 (8)	399 ± 4
Andis9	1400	0.6	0.1 (8)	144 ± 5
<i>Low-Ti (A15 Yellow Glass) + 10% olivine</i>				
Andis12	1300	0.6	2.0 (12)	495 ± 10
Andis13	1250	0.6	0.5 (23)	172 ± 20

^a Numbers in parenthesis are duration of anorthosite synthesis run.

^b One standard deviation estimated from 5 measurements around the central portion of a given charge.

Approximately cylindrical picritic glass and anorthosite rods were first synthesized separately using the C–Pt–Mo capsule at the same temperature and pressure as the actual dissolution experiments (1250–1400 °C, 0.6 GPa, 4–8 h for the picritic glasses and 8–24 h for the anorthosite, Table 2). After each synthesis run the molybdenum capsule was cut in half perpendicular to the cylindrical axis using a low speed diamond-wafering saw. The exposed surface was polished. The polished samples were then stored in a vacuum oven at 200 °C for at least 12 h to remove water that may have entered the capsule during the polishing.

The dissolution couple was made by juxtaposing 1/2 of a pre-synthesized anorthosite rod on top of 1/2 of a pre-synthesized picritic glass rod in the C–Pt–Mo capsule. A thin platinum sleeve was then placed around the dissolution couple. Platinum alloys with molybdenum at the run conditions and helps to prevent the two halves of the dissolution couple from separating upon decompression. The furnace assembly was then stored in a vacuum oven at 110 °C for at least 12 h. To conduct a dissolution run the charge was first cold pressurized to a pressure about 10–20% higher than the desired run pressure. The temperature was raised to 1000 °C at 75 °C/min, while maintaining the pressure at the prescribed run pressure (hot-piston in). After a 2 h pre-anneal at 1000 °C the temperature was then raised to the run temperature (1250–1420 °C) at 150 °C/min. At the end of the run, the temperature was dropped to 600 °C by a step change in temperature with no attempt to maintain the pressure. The charge was then held at 600 °C for ~2 min before a final quench to room temperature. The quenched capsules were sectioned longitudinally, polished, and mounted for electron microprobe analysis. A slight difference in diameters between the two half cylinders containing the pre-synthesized materials (due to deformation during the synthesis run) results in a

small offset at the original rock-melt interface and thus serves as a marker for distance measurements (Fig. 2). Table 2 lists the conditions used for all of the anorthosite dissolution experiments.

In all experiments the temperature was measured with a W₉₇Re₃–W₇₅Re₂₅ thermocouple and a Eurotherm 818 controller. No pressure correction was applied to the measured e.m.f. Uncertainties in temperature measurements are about 10 °C, due mainly to the presence of a temperature gradient in the furnace (e.g., Ayers et al., 1992; Liang et al., 1996). The nominal pressure was not corrected for friction because pressure fluctuations during a typical run (~30 MPa) were comparable to the friction correction measured by Ayers et al. (1992) for a similar furnace assemblage (~25 MPa).

2.3. Dissolution distance measurements

Backscattered electron (BSE) images were used to measure the dissolution distance. The dissolution distance is simply the distance between the original interface and the current interface. To avoid the complications resulting from the small offset at the original interface the dissolution distances were measured around the center of the charge a minimum of 5 times for each sample. The average measurements are reported in Table 2.

2.4. Microprobe analysis

Chemical analyses were conducted using a Cameca SX100 electron microprobe at Brown University. The analytical conditions for the glass were an accelerating voltage of 15–20 kV, and a beam current of 15–25 nA. A focused beam was used for glass analyses in quench-crystal-free

glasses such as experiments dissolving anorthosite into VLT picritic glasses (runs Andis2 and Andis3). For the low-Ti and high-Ti glass experiments containing abundant quench growth, a 20–25 μm diameter beam was used for glass analyses in quench-crystal-bearing glasses (Andis4, Andis5, and Andis13). Counting times were 10–30 s for peak and 10–15 s for background positions. Natural mineral standards were used and the ZAF matrix correction was employed.

3. Results

Anorthosite dissolution in lunar picritic magmas was explored as a function of temperature and melt composition. The starting lunar picritic magmas are synthetic versions of a very low-Ti Apollo 15 green glass, a low-Ti Apollo 15 yellow glass, an olivine-saturated low-Ti melt, and a high-Ti Apollo 15 red glass (Table 1).

3.1. Types of anorthosite dissolution reactions

We conducted three types of anorthosite dissolution experiments, designated as cases C1, C2, and C3 in Fig. 1. The first type of experiment is anorthosite dissolution into a crystal-free magma at 1400 °C (case C1). The starting liquid composition is specified by the X in Fig. 1, the anorthite composition by the filled circle, and the interface melt composition by the open circle. Case C2 illustrates lower temperature experiments (1250–1300 °C) in which spinel crystallized from the melt near the anorthosite interface. And case C3 represents experiments conducted at 1250–1300 °C but with 10% olivine added to the low-Ti glass to ensure olivine saturation.

The experiments dissolving anorthosite into an initially olivine-saturated liquid (case C3) produced a spinel + liquid region and a crystal-free region (Fig. 2a). The development of the spinel + liquid region as well as the crystal-free region can be explained with the help of Fig. 1 (cases C1 and C3). The composition of the melt at the interface with the anorthosite is approximately in equilibrium with anorthite, but the composition varies away from the interface, becoming more enriched in the olivine components, moving the composition into the spinel + liquid region. As the Fo content of the liquid increases the bulk liquid composition enters the crystal-free melt, before entering the olivine + melt region.

In all 1250 and 1300 °C experiments spinel was stabilized in the melt next to the picritic magma-anorthosite interface. The morphology of the spinel-rich region has a waviness to it, suggestive of a Rayleigh–Taylor instability (Figs. 2 and 3; Michioka and Sumita, 2005). In the 1 and 2 h spinel-bearing experiments (Andis11 and Andis12) the spinel + liquid region developed drips that extend below the original interface (Fig. 3).

In the 1400 °C anorthosite dissolution experiments corresponding to case C1 in Fig. 1a, the anorthosite simply dissolves into the crystal-free melt without spinel crystalli-

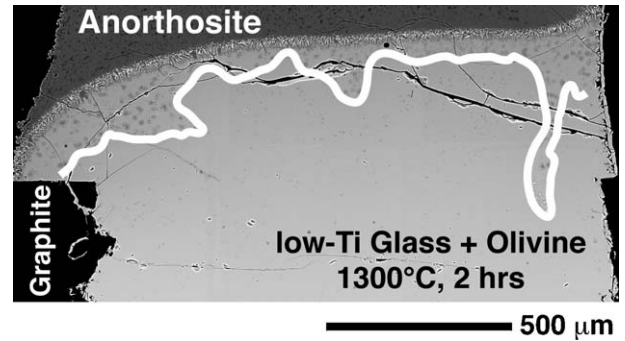


Fig. 3. BSE image of anorthosite dissolution into a low-Ti picritic magma (Andis12, 1300 °C, 0.6 GPa, 2.0 h). The white line drawn on the image marks the bottom boundary of the spinel + liquid region. Note the fingering morphology resulting from Rayleigh–Taylor instability.

zation or olivine dissolution. At the anorthosite-melt interface a 22–185 μm thick layer of anorthite quench crystals developed.

3.2. Anorthosite dissolution rate

Fig. 4 is a plot of our measured dissolution distances as a function of the square root of time. The parabolic growth kinetics (linear in this plot) for the short duration dissolution experiments (≤ 1 h, Fig. 4) are consistent with diffusive dissolution in a semi-infinite geometry (Zhang et al., 1989; Liang, 1999, 2000, 2003). At later times, diffusion modifies the composition of the picritic melt throughout the capsule

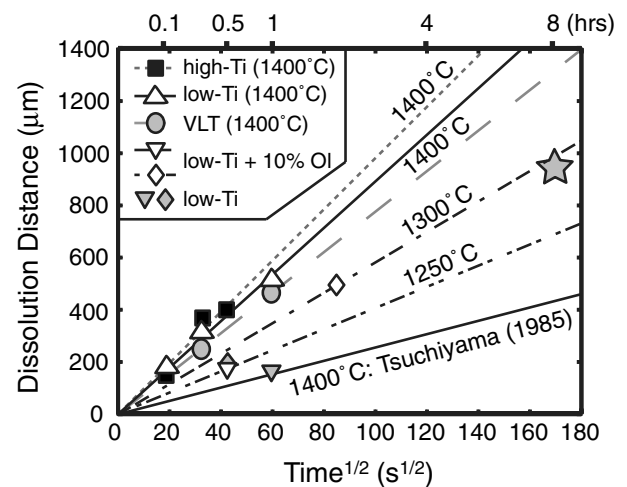


Fig. 4. Plot of measured dissolution distance against the square root of time. The actual measurements are the symbols and the lines are best fit to the data. The measurement errors are smaller than the size of the symbols. The star is a VLT dissolution experiment Andis1 (1420 °C, 0.6 GPa, 8 h) where the experimental duration was long enough that diffusion has modified the composition of the far field melt. The open upside down triangle (open diamond) is an anorthosite dissolution experiment in the low-Ti magma doped with 10% olivine at 1250 °C (1300 °C). The filled upside down triangle (filled diamond) is an anorthosite dissolution experiment in the low-Ti magma at 1250 °C (1300 °C). For comparison the lower line is for anorthite dissolution in a terrestrial andesite liquid from Tsuchiyama (1985).

reducing the dissolution rate, as illustrated by the 8 h dissolution experiment (star in Fig. 4, 1420 °C and 0.6 GPa, also see Fig. 3b of Liang, 2003). Fig. 4 shows that the rate of anorthosite dissolution in the lunar picritic magmas is considerably faster than the rate of plagioclase dissolution in a terrestrial andesite (1400 °C and 1 bar, Tsuchiyama, 1985).

The dissolution rates for the three sets of 1400 °C experiments are the best constrained with 2 or 3 dissolution experiments. For comparison, we have also included our lower temperature dissolution runs (1250 and 1300 °C) in which 10% olivine was added to the low-Ti magma to force olivine saturation (Andis12 and Andis13). The filled triangle and diamond in Fig. 4 are anorthosite dissolution experiments conducted in the low-Ti magma without olivine addition, but at the same pressure and temperature. As expected the addition of normative olivine to the low-Ti magma drives the melt farther away from equilibrium with the anorthosite, increasing the dissolution rate.

Fig. 5 is a plot of the anorthosite diffusive dissolution rate in the VLT, low-Ti, and high-Ti magmas as a function of temperature. The points at 1400 °C are an average of the 2 or 3 experiments and all other points are from single runs. The experiments conducted in the low-Ti magma over a range in temperatures allow us to estimate an apparent activation energy for the anorthosite dissolution reactions. From a linear least squares analysis of the low-Ti dissolution rates we obtained an apparent activation energy of $166 \pm 17 \text{ kJ mol}^{-1}$ for the dissolution reaction. Our estimated activation energy for anorthosite dissolution in the low-Ti magma is within the range of self diffusion of Si (181 kJ mol^{-1}), Ca and Mg (143 kJ mol^{-1} and 148 kJ mol^{-1} , respectively) in a diopside melt (Shimizu

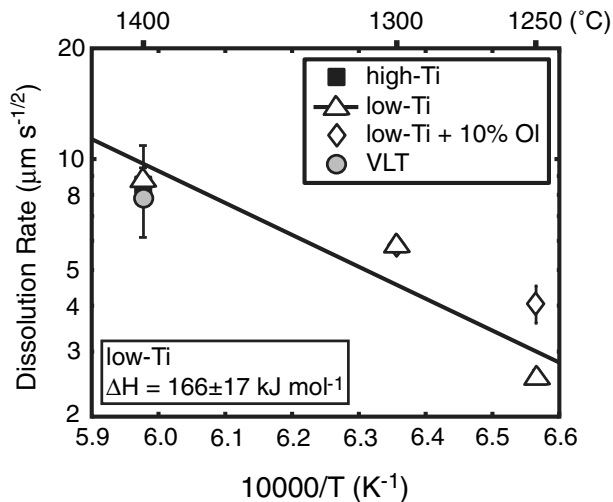


Fig. 5. Plot of measured diffusive dissolution rate in the low-Ti magma against the normalized temperature ($10000/T$). The symbols at 1400 °C are the average of 2 or 3 measurements with the error bars representing 1 standard deviation about the mean. All other symbols are single measurements of the dissolution rate, with the error bars representing measurement errors. The line is an exponential fit to the low-Ti data. The activation energy ΔH ($166 \pm 17 \text{ kJ mol}^{-1}$) is calculated from the exponential fit and the error is one standard deviation.

and Kushiro, 1991) and is consistent with chemical diffusion of CaO (192 kJ mol^{-1}) and SiO₂ (217 kJ mol^{-1}) in a CAS liquid when the melt compositions are adjusted (45wt% SiO₂, 35% CaO, 20% Al₂O₃; Liang and Davis, 2002). This suggests that anorthosite diffusive dissolution is rate-limited by chemical diffusion of the major elements in the melt.

3.3. Melt chemistry

The concentration profiles developed during anorthosite dissolution are similar to those seen in previous diffusive dissolution studies (e.g., Watson, 1982; Zhang et al., 1989; Finnila et al., 1994; Liang, 1999, 2003; Morgan and Liang, 2003, 2005). Fig. 6 is a plot of melt concentration as a function of position for anorthosite dissolution into the VLT, low-Ti and high-Ti picritic magmas. The concen-

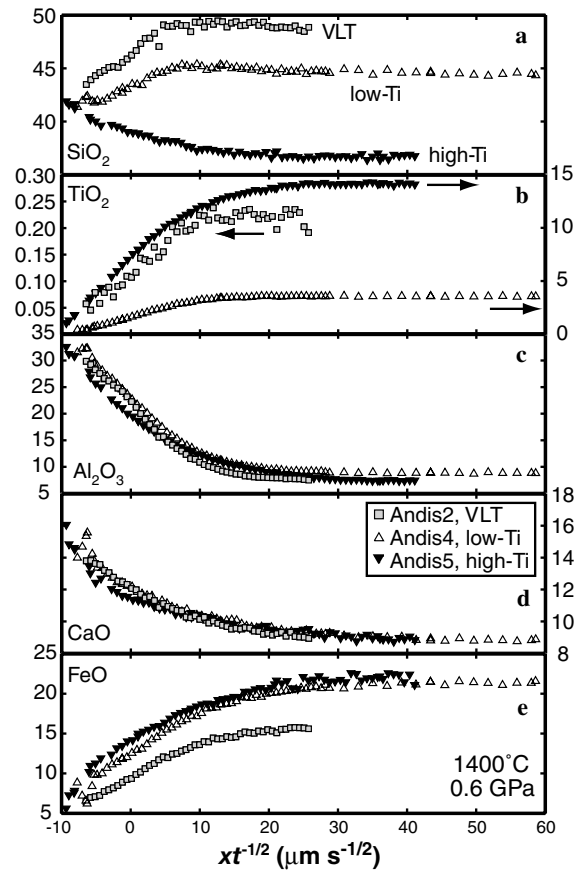


Fig. 6. Plots of concentration profiles resulting from anorthosite dissolution into VLT, low-Ti and high-Ti picritic glasses. The concentrations are in weight percent. The profiles are Andis2 (VLT glass, gray filled squares; 1.0 h), Andis4 (low-Ti glass, open triangles; 0.3 h), and Andis5 (high-Ti glass, black upside down triangles; 0.3 h). All three experiments were conducted at 1400 °C and 0.6 GPa. The scale for TiO₂ in the VLT experiments has been expanded to make it visible (Y-axis on the left in panel b). The scale for TiO₂ in the low-Ti and high-Ti runs is shown on the right of panel b. The arrows point toward the TiO₂ profiles respective axes. The positions have been normalized to compare the profiles from experiments run for different times. The original interface between the anorthosite and the picritic glasses was at position 0.

tration profiles illustrate the similarities and differences resulting from anorthosite dissolution into 3 distinct picritic melt compositions. The profiles for CaO and Al₂O₃ in the melt are similar for all three reacting melt compositions with high concentrations at the interface with the anorthosite (Fig. 6). The different shapes of the CaO and Al₂O₃

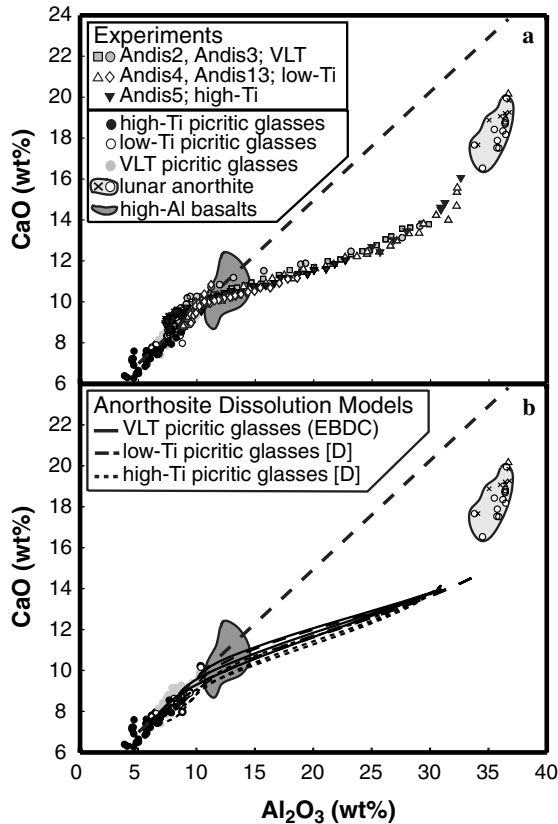


Fig. 7. Plot of CaO vs. Al₂O₃ for the picritic glasses, high-Al basalts, lunar anorthite compositions, (a) concentration profiles resulting from anorthosite dissolution; and (b) calculated concentration profiles of anorthosite dissolution into the picritic glasses. The filled black circles are the high-Ti picritic glasses (Delano, 1986; Shearer and Papike, 1993); the black open circles are the low-Ti picritic glasses (Delano, 1986; Hughes et al., 1988; Shearer and Papike, 1993); the filled gray circles are the VLT picritic glasses (Delano, 1986; Shearer and Papike, 1993; Elkins et al., 2000). The thick dashed line is a linear regression to all of the reported picritic glass data extrapolated to 35% Al₂O₃. The field corresponds to the high-Al basalts (Dickinson et al., 1985; Neal et al., 1989). The open gray circles and the crosses correspond to the lunar anorthite compositions, where the circles are from Papike et al. (1996), the crosses are from Shervais and McGee (1998), and the open triangle is the pure anorthite used in our experiments. Profiles resulting from the anorthosite dissolution experiments are runs Andis2 and Andis3 (VLT picritic glasses, filled gray squares and circles, respectively), Andis4 and Andis13 (low-Ti picritic glasses, open triangles, and diamonds, respectively), and Andis5 (high-Ti picritic glass, filled upside down triangles). The low-Ti and high-Ti profiles were calculated using Eqs. A3 in Appendix A, the diffusion matrices reported in Table 3, and a series of different initial melt compositions. The VLT profile was modeled using the EBDCs estimated from the low-Ti diffusion matrix. The initial melt compositions were chosen to correspond to the low, intermediate, and high CaO and Al₂O₃ contents for each class of picritic glasses. The solid composition and the interface melt compositions were similar to our experiments.

profiles (i.e., Al₂O₃ is steeper) are primarily due to the different rates of diffusion in the melt (e.g., Watson, 1982; Zhang et al., 1989; Liang, 1999, 2003). The profiles for FeO and TiO₂ increase from the low concentration at the anorthosite-melt interface into the unmodified melt. The profiles for SiO₂ depend on the composition of the reacting melt. In the high-Ti picritic magma (Andis5), the SiO₂ profile decreases monotonically from the anorthosite-melt interface to 37% at the far field. In contrast, the SiO₂ profiles in the VLT and low-Ti picritic magmas (Andis2 and Andis4, respectively) show a pronounced feature resulting from uphill diffusion, i.e., diffusion against its own concentration gradient (e.g., Zhang et al., 1989; Watson and Baker, 1991; Liang et al., 1996, 1997; Richter et al., 1998).

Fig. 7a is a plot of CaO vs. Al₂O₃ in the reacting melts from our dissolution experiments. Fig. 8a is a ternary plot of MgO, TiO₂, and Al₂O₃ in the same melts. Diffusive dissolution produces nonlinear concentration profiles when viewed in element correlation diagrams. The nonlinear profiles are directly related to differences in the chemical diffusivities of the oxide components in the melt.

3.4. Melt density and viscosity

Melt density and viscosity depend strongly on its composition. Fig. 9 displays the calculated melt density and viscosity for runs Andis2 (VLT), Andis4 (low-Ti) and Andis5 (high-Ti). The density and viscosity were calculated from their compositions using the formulations of Lange and Carmichael (1990) and Shaw (1972), respectively. The high-Ti magma has the lowest viscosity and highest density (0.17 Pa s and 3110 kg m⁻³), the VLT magma has an intermediate viscosity and the lowest density (0.61 Pa s and 2880 kg m⁻³), and the low-Ti magma has the highest viscosity and an intermediate density (0.64 Pa s and 2970 kg m⁻³) at 1400 °C (Fig. 9). Recorded in the composition profiles are systematic variations in melt density from a minimum of approximately 2750 kg m⁻³ near the anorthosite-magma interface to the respective unmodified magma densities. Similarly, the magma viscosities also vary as a function of position, with the maximum viscosity of approximately 3 Pa s near the anorthosite-magma interface and decreasing to the unmodified magma viscosities of 0.2–0.6 Pa s (Fig. 9b).

4. Kinetics of anorthosite dissolution in lunar picritic magmas

The anorthosite dissolution rates are a function of the transport properties of the magma (i.e., diffusivities and viscosity) and the extent of undersaturation of anorthite in the dissolving liquids (e.g., Zhang et al., 1989; Liang, 1999). From the concentration profiles developed in the anorthosite dissolution experiments we can estimate the diffusivities of the oxide species in the melt.

The simplest method of describing diffusion in a multi-component system is the effective binary diffusion approach whereby coupled chemical diffusion is simplified

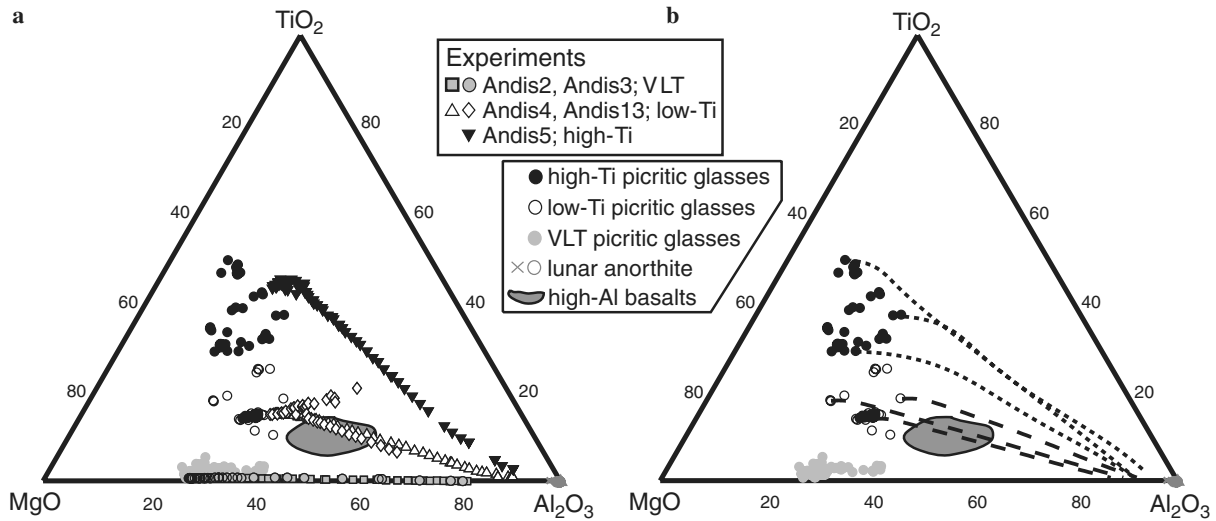


Fig. 8. Ternary diagram of MgO, TiO₂, and Al₂O₃ for the picritic glasses, high-Al basalts, lunar anorthosite compositions. (a) Concentration profiles resulting from anorthosite dissolution; and (b) calculated concentration profiles for anorthosite dissolution into the picritic glasses. The symbols and parameters used to generate the profiles are the same as those used in Fig. 7. Note that the low-Ti picritic profile overlaps the measured high-Al basalt compositions.

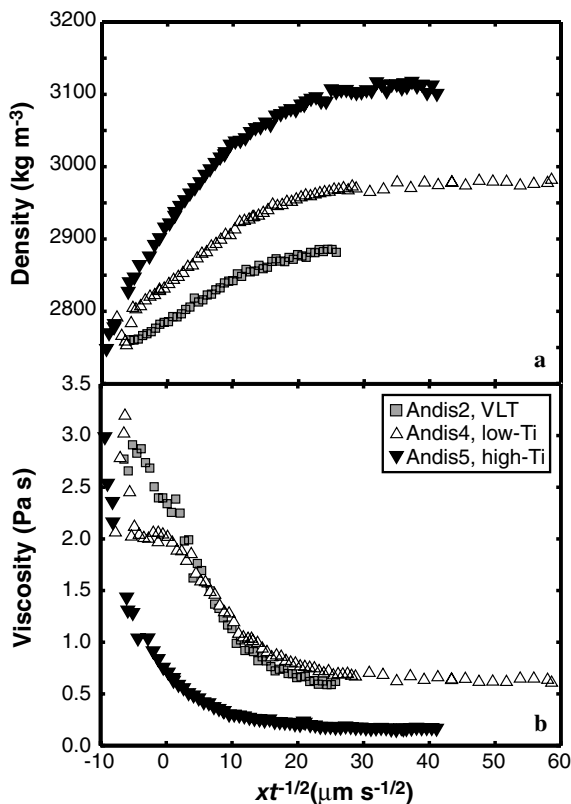


Fig. 9. Plots of calculated melt density and viscosity as a function of position in the dissolution charge. The samples used in the calculation are Andis2 (VLT glass, gray filled squares; 1.0 h), Andis4 (low-Ti glass, open triangles; 0.3 h), and Andis5 (high-Ti glass, black upside down triangles; 0.3 h). All three experiments were conducted at 1400 °C and 0.6 GPa. The densities were calculated using the method of Lange and Carmichael (1990). The viscosities were calculated using the method of Shaw (1972). The positions have been normalized to compare the profiles from experiments run for different times. The original interface between the anorthosite and the picritic glasses was at position 0.

by an effective binary diffusion coefficient (EBDC, e.g., Cooper, 1968; Watson, 1982; Zhang et al., 1989; also see Eq. (1a) below). As a first step we tried modeling the concentration profiles shown in Fig. 6 using the effective binary approach. However, the concentration profiles developed during anorthosite dissolution show uphill diffusion in SiO₂ that cannot be accounted for by an EBDC (dashed line in Fig. 10a). To include SiO₂ in our model calculations, we expand the effective binary approach by introducing an effective diffusion matrix. In this expanded, yet still simplified approach, we take MgO as the dependent variable and allow the diffusive flux of SiO₂, Al₂O₃, or TiO₂ to couple with the concentration gradients of CaO and FeO. For simplicity we also assume that diffusive couplings among SiO₂, Al₂O₃, and TiO₂ are negligibly small compared to their respective diagonal terms. These simplifications are consistent with the observed diffusive coupling behaviors in the ternary CaO–Al₂O₃–SiO₂ and MgO–Al₂O₃–SiO₂, and quaternary CaO–MgO–Al₂O₃–SiO₂ systems (Liang et al., 1996; Richter et al., 1998). The effective diffusion matrices reported below, though incomplete, contain the minimum number of components needed to adequately describe the first order diffusive behavior of the multicomponent system.

To proceed, we follow the methods of Liang (1999) for diffusive dissolution in molten silicates to estimate the effective diffusion matrices for the low-Ti and high-Ti picritic magmas. The exact solution for diffusive dissolution in our simplified system is outlined in Appendix A. The diffusion matrices for the low-Ti and high-Ti melts were inverted from the concentration profiles using the Levenberg–Marquardt method and Eqs. (A.3a)–(A.3c) in Appendix A. Because diffusion clearly modified the far field melt composition in the VLT dissolution experiment (Andis2) we could not estimate the diffusion matrix for

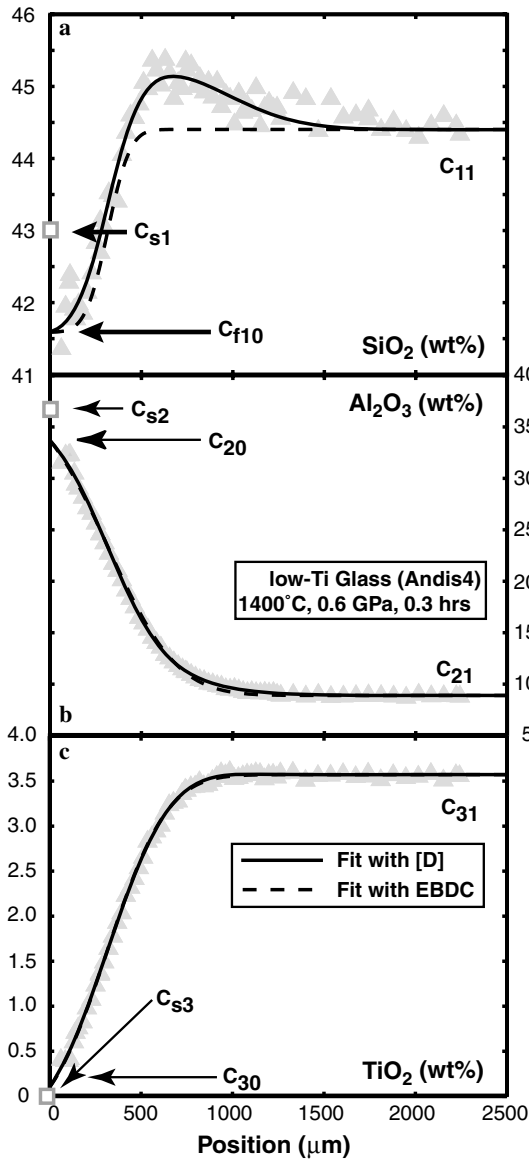


Fig. 10. Plot of measured SiO_2 , Al_2O_3 , and TiO_2 concentration profiles resulting from anorthosite dissolution into the low-Ti magma at 1400°C and 0.6 GPa for 0.3 h . The triangles are the measured compositions. The solid lines are fits to the data using the estimated multicomponent diffusion matrix. The dashed lines are fits to the data using the effective binary diffusion coefficients in the low-Ti magma. C_{11} , C_{21} and C_{31} correspond to the initial low-Ti SiO_2 , Al_2O_3 , and TiO_2 contents, respectively. C_{10} , C_{20} , and C_{30} correspond to the interface melt SiO_2 , Al_2O_3 , and TiO_2 contents, respectively. C_{s1} , C_{s2} , and C_{s3} correspond to the anorthosite SiO_2 , Al_2O_3 , and TiO_2 contents, respectively. The positions have been corrected to put the anorthosite-glass interface at position $0\ \mu\text{m}$. The square at position $0\ \mu\text{m}$ is the anorthosite composition.

this melt. Table 3 shows diffusion matrices estimated for the low-Ti and high-Ti picritic magmas. The relatively large uncertainties associated with the off diagonal terms of the diffusion matrices are due mainly to the fact that our reported diffusion matrices in Table 3 were inverted from diffusive dissolution experiments conducted along only one direction in compositional space (e.g., Liang, 1994; Trial and Spera, 1994). Fig. 10 compares the mea-

sured and calculated concentration profiles of SiO_2 , Al_2O_3 , and TiO_2 resulting from anorthosite dissolution in the low-Ti magma using the diffusion matrix (solid lines) and the EBDCs (dashed lines) listed in Table 3.

The relative strength of diffusive coupling can be estimated by comparing the magnitude of the product of the diagonal terms $|D_{ii}\Delta C_i|$ with the off diagonal terms $|D_{ij}\Delta C_j|$ (Liang, 1994, 1999), where D_{ii} and D_{ij} are the diagonal and off diagonal terms of the diffusion matrix, respectively; ΔC_i and ΔC_j are the composition differences for component i and j , respectively. If the magnitudes of the product of the off diagonal terms are comparable to or larger than those of the diagonal terms, coupled diffusion is important. In this way we find strong diffusive coupling of TiO_2 , Al_2O_3 and SiO_2 with CaO and FeO in both the low-Ti and high-Ti dissolution experiments. Our dissolution experiments and estimated diffusion matrices show that the simpler EBDC approach to modeling the interactions of SiO_2 between the picritic magmas and the anorthosite is inadequate and the use of an effective diffusion matrix is required.

In order to compare our measured diffusivities with those of the previous studies (e.g., Finnilla et al., 1994) we estimated EBDCs from our diffusion matrix. To estimate the EBDCs we note that the net flux of component i for multicomponent diffusion must equal to the Fick's law flux for component i . We use the following expression to estimate the EBDCs (Cooper, 1968):

$$D_i^E \frac{\partial C_i}{\partial x} = D_{i-\text{CaO}} \frac{\partial C_{\text{CaO}}}{\partial x} + D_{i-\text{FeO}} \frac{\partial C_{\text{FeO}}}{\partial x} + D_{ii} \frac{\partial C_i}{\partial x}, \quad (1a)$$

$$\frac{\partial C_i}{\partial x} = \frac{C_{i1} - C_{i0}}{L}, \quad (1b)$$

where D_i^E is the EBDC of component i ; $D_{i-\text{CaO}}$ and $D_{i-\text{FeO}}$ are coupled diffusion coefficients (Table 3); D_{ii} is the diagonal term of the diffusion matrix (Table 3); L is the diffusive length scale; i is the species of interest (Al_2O_3 , TiO_2 or SiO_2); C_{i1} is the initial concentration of species i in the melt, and C_{i0} is the concentration of species i at the interface with the anorthosite. As shown in Table 3, our estimated EBDC for Al_2O_3 is $4.5 \times 10^{-11}\text{ m}^2\text{ s}^{-1}$ for the low-Ti glass and $6.8 \times 10^{-11}\text{ m}^2\text{ s}^{-1}$ for the high-Ti glass, which are approximately the same order of magnitude as the EBDC of Al_2O_3 found by Finnilla et al. (1994) in their FeO-free system at approximately the same temperature. The estimated EBDCs for TiO_2 , Al_2O_3 and SiO_2 in the high-Ti magma are slightly larger than those of the low-Ti magma, whereas the EBDCs for CaO and Al_2O_3 in the low-Ti magma are slightly larger than those in high-Ti magma.

The dissolution rate depends on the transport properties of the melt (e.g., diffusivities and viscosity), the thermodynamic driving force, and the style of dissolution (convective vs. diffusive). The chemical potential gradients driving anorthite dissolution are related to the degree of undersaturation of the dissolving magma with respect to anorthite. To compare our measured anorthosite dissolution rates

Table 3
List of chemical diffusion coefficients taking MgO as the dependent variable^a

D_{i-j}	$D_{i-\text{CaO}}$	$D_{i-\text{FeO}}$	$D_{i-\text{TiO}_2}$	$D_{i-\text{Al}_2\text{O}_3}$	$D_{i-\text{SiO}_2}$	EBDC ^c
<i>Low-Ti (Andis4; 1400 °C, 0.6 GPa, 0.3 h)</i>						
$D_{\text{CaO}-j}$	8.3 ± 0.7^b	0	0	0	0	8.3 (8.3)
$D_{\text{FeO}-j}$	0	7.9 ± 0.4	0	0	0	7.9 (7.9)
D_{TiO_2-j}	-5.2 ± 11	-2.3 ± 4.4	3.9 ± 0.8	0	0	2.9 (3.1)
$D_{\text{Al}_2\text{O}_3-j}$	28 ± 49	7.3 ± 20	0	2.3 ± 0.5	0	4.5 (4.1)
D_{SiO_2-j}	86 ± 22	32 ± 8.6	0	0	0.90 ± 0.3	NA
<i>High-Ti (Andis5; 1400 °C, 0.6 GPa, 0.3 h)</i>						
$D_{\text{CaO}-j}$	7.6 ± 0.8	0	0	0	0	7.6 (7.6)
$D_{\text{FeO}-j}$	0	6.7 ± 0.4	0	0	0	6.7 (6.7)
D_{TiO_2-j}	3.1 ± 15	3.8 ± 6.2	1.7 ± 0.8	0	0	4.6 (4.3)
$D_{\text{Al}_2\text{O}_3-j}$	140 ± 42	46 ± 17	0	2.8 ± 1.2	0	6.8 (5.3)
D_{SiO_2-j}	6.7 ± 26	2.2 ± 11	0	0	3.6 ± 5.2	4.6 (4.1)

^a Diffusion coefficients in $\times 10^{-11} \text{ m}^2 \text{ s}^{-1}$.

^b $\pm 1\sigma$ errors are calculated directly from each inversion.

^c Effective binary diffusion coefficients (EBDC) estimated from the diffusion matrix. The numbers in the parenthesis are the EBDC calculated using the approach of Zhang et al. (1989).

with that reported by Tsuchiyama (1985) we use the degree of undersaturation defined by Zhang et al. (1989) and Liang (1999):

$$\Theta = \frac{C_{10} - C_{11}}{C_{s1} - C_{10}}, \quad (2)$$

where C_{11} is the concentration of the reference species in the unmodified melt; C_{s1} is the concentration in the solid; and C_{10} is the concentration in the interface melt (see Fig. 10 for a definition of the symbols). Assuming Al_2O_3 is the rate-limiting species the degree of undersaturation ranges from 6.6 to 7.1 for the lunar picritic magmas relative to 0.2 for the andesitic composition of Tsuchiyama (1985). Hence, the faster anorthite dissolution in the lunar picritic magmas is at least in part due to the larger degree of undersaturation of the picritic magmas with respect to anorthite.

Diffusive dissolution is not the dominant mechanism of mass transfer during anorthosite assimilation on the moon. Magma flowing through or stored in the crust can assimilate anorthosite more efficiently by melting and/or convective dissolution. Convective dissolution is characterized by a boundary layer separating the solid from the well-mixed melt. Within the boundary layer, mass transfer is dominated by diffusion. As a consequence the chemical variations resulting from convective dissolution are approximately the same as diffusive dissolution (Cussler, 1997). The rates of convective dissolution are expected to be greater than the rates of diffusive dissolution. The rates of convective dissolution can be estimated using the simple expression (e.g., Zhang et al., 1989; Kerr, 1995):

$$V = \frac{D_f^E}{\delta} \Theta, \quad (3)$$

where V is the convective dissolution rate (m/s); D_f^E is the EBDC of the rate-limiting species in the melt (m^2/s); δ is the boundary layer thickness (m); and Θ is the degree of undersaturation defined in Eq. (2). The boundary layer

thickness can be approximated using the expression (Cussler, 1997):

$$\delta = \frac{d}{Sh}, \quad (4)$$

where d is the diameter of the melt filled tube and Sh is the Sherwood number. The dimensionless Sherwood number is a measure of the rate of total mass transfer to the rate of pure diffusive mass transfer (e.g., Cussler, 1997):

$$Sh = \frac{kl}{D_f^E}, \quad (5)$$

where k is the mass transfer coefficient (m/s); and l is the length scale (m). Mass transfer coefficients depends strongly on the physical properties of the fluid as well as the styles of fluid–solid interaction. Fig. 11 plots the rates of convective dissolution as a function of the degree of undersaturation (Θ) and the Sherwood number. The following parameters were used to calculate the mass transfer coefficient (k) in the boundary layer thickness calculation and are consistent with dike analysis for the moon: an initial dike diameter of 5 m, pipe length of 60 km, a melt velocity of 0.5 m s^{-1} (Wilson and Head, 2003) and the densities and viscosities from Fig. 9. Using these parameters, we found the boundary layer thickness for the picritic magmas are 0.6% and 0.01% of the dike diameter for laminar flow and turbulent flow in a tube, respectively. The degree of undersaturation (Θ) ranged from 6.6 to 7.1 for the picritic glasses reported in Table 1. The rates of convective dissolution during laminar and turbulent flow in a tube are approximately a factor of 2 and 10 times larger than the rates of diffusive dissolution, respectively.

The results of these calculations suggest that the lunar picritic magmas are capable of assimilating significant amounts of lunar crustal materials. However, relative to the amount of melt flowing in a dike the total amount anorthite assimilated is small and the total effect on magma chemistry will be relatively small, which is consistent with

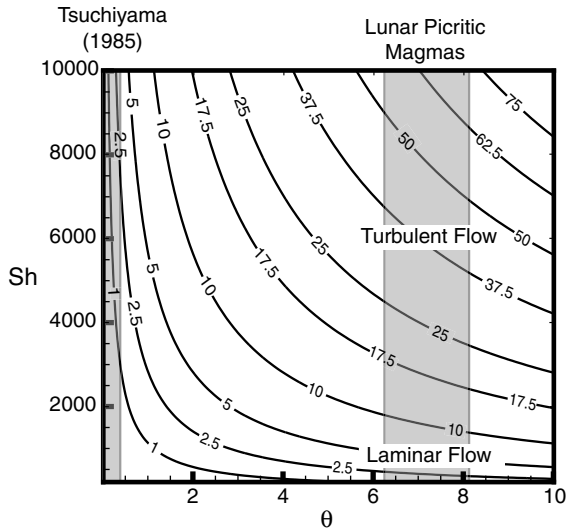


Fig. 11. Contour plot of anorthosite convective dissolution rate (in units of 10^{-8} m s^{-1}) as a function of the degree of undersaturation (θ) and the Sherwood number (Sh). The degree of undersaturation is defined by Eq. (2) and the Sherwood number is defined by Eq. (5). The lunar picritic magmas field is defined by calculating the degree of undersaturation for the picritic glasses reported by Delano (1986), Hughes et al. (1988), Shearer and Papike (1993) and Elkins et al. (2000) and by calculating the Sherwood number for laminar and turbulent flow in a tube (Cussler, 1997). The field Tsuchiyama (1985) is defined by calculating the degree of undersaturation for their anorthosite dissolution in a terrestrial andesite composition.

previous work on anorthosite assimilation (Finnila et al., 1994).

5. Consequences of anorthosite assimilation in lunar magmas

5.1. Lunar picritic magmas

Aside from the thermal constraints, a key to Finnila et al.'s (1994) argument is the trend in the picritic glass compositions. Finnila et al. (1994) observed that there is a well-defined trend of increasing CaO and Al_2O_3 in the picritic glass compositions. We have reproduced the plot of CaO vs. Al_2O_3 including a greater number of picritic glass compositions in Fig. 7 (Delano, 1980, 1986; Hughes et al., 1988; Shearer and Papike, 1993; Elkins-Tanton et al., 2003). When extrapolated to Al_2O_3 concentrations consistent with anorthite, the trend defined by Finnila et al. (1994) does not intersect the measured lunar anorthite compositions. Instead, it extends to higher CaO contents than the pure anorthite endmember, making the apparent misfit even worse when compared with actual lunar anorthite compositions (light hatched field in Fig. 7). While the study of Finnila et al. (1994) explored anorthosite assimilation by dissolution as well as melting, they did not explore how the different mechanisms would add the dissolved anorthite components to the melt. As shown in Fig. 7, the composition profiles are not a simple linear mixture of the two endmembers, instead more complicated nonlinear profiles are developed. The nonlinear trend

resulting from diffusive dissolution of anorthosite (and precipitation of spinel) diverges from the picritic glass derived best fit line and connects the initial picritic glass compositions to anorthite compositions.

Fig. 8 shows the covariation of MgO , TiO_2 , and Al_2O_3 in ternary composition space that illustrates the composition profiles developed between anorthite and the initial magma compositions in our dissolution experiments. If we consider all of the picritic glasses as a group they define a trend of increasing TiO_2 with relatively large scatter in the MgO and Al_2O_3 abundance of the picritic glasses at a constant TiO_2 may result from anorthosite assimilation. We speculate that the picritic glasses with the lowest Al_2O_3 contents experienced the least amount of anorthite addition, while the picritic glasses with the highest Al_2O_3 contents experienced the most.

There are numerous picritic glass compositions and we have explored anorthosite dissolution into only three different picritic melts in our experiments. Our results were extended to a greater variety of starting picritic glass compositions using the exact solution for mineral dissolution from Appendix A (Eqs. (A.3a)–(A.3c)) and the estimated effective diffusion matrix from Table 3. Since an effective diffusion matrix for the VLT melt is not available, we used the EBDCs estimated from the low-Ti magma to generate approximate concentration profiles for anorthosite dissolution in the VLT glasses. We chose three compositions from each of the VLT, low-Ti and high-Ti picritic glasses. The three initial compositions chosen correspond to a low, an intermediate, and a high CaO and Al_2O_3 composition glass. Lacking better phase equilibria data we assume the composition of melt in equilibrium with anorthite is approximately the same as our experimental compositions when extrapolated to the anorthosite-melt interface. The results of these calculations are shown as dashed or solid lines in Figs. 7b and 8b. For clarity, our measured dissolution profiles were left off, but the other lunar data is included for comparison. Even when picritic glass compositions are changed, the profiles remain qualitatively the same. With these simplified models, we can produce an entire field of compositional profiles that are similar to our experimental results yet still remain chemically restricted in plots of CaO vs. Al_2O_3 (Fig. 7b).

5.2. High-Al basalts

An interesting application of our anorthosite assimilation experiments is the origin of the high-Al basalts. Previous models for the petrogenesis of the high-Al basalts have primarily focused on partial melting, fractional crystallization, assimilation or some combination of these processes (Dickinson et al., 1985; Shervais et al., 1985; Neal and Taylor, 1988, 1990; Neal et al., 1989). Dickinson et al. (1985) proposed a model that combines partial melting of a predominantly olivine + pyroxene source coupled with assimilation of a KREEP rich material. Neal et al. (1989) suggested a model that involves assimilation of KREEP

and fractional crystallization. Here, we focus on the systematics of the major elements in high-Al basalt.

In Figs. 7 and 8 we include the high-Al basalt compositions reported by Dickinson et al. (1985), Neal et al. (1989) and Neal and Taylor (1990). Assuming that the initial liquids parental to the high-Al basalts have chemical trends similar to the picritic glasses, then it is feasible that the composition of high-Al basalts result, at least in part, from anorthosite assimilation. In the plots of CaO vs. Al₂O₃, anorthite assimilation starting with an initial liquid similar to picritic glass in composition results in profiles passing through the high-Al basalt field (Figs. 7a and b). However, when the plots include other components, only the low-Ti picritic glass compositions pass through the high-Al basalt field (Figs. 8a and b). The limited TiO₂ variability may be the result of the small population size or a common source region for all of the high-Al basalts (Dickinson et al., 1985; Neal et al., 1989, Neal and Taylor, 1990). In our experiments with an olivine-saturated magma reacting with the anorthosite, the combination of olivine modification of the melt coupled with anorthosite assimilation results in a composition profile that almost perfectly fits the observed high-Al basalt compositions. The concentration profile starts within the olivine + picritic magma field as predicted by the phase diagram, then passes into a crystal-free region, and then into the melt + spinel region before reaching the interface with the anorthosite (Figs. 1, 7, and 8).

5.3. Spinel in lunar basalts and picritic magmas

Spinel growth during the reaction between anorthosite and picritic magmas may be additional evidence for the interaction of the lunar magmas with anorthositic crust. Spinel is a minor but apparently ubiquitous phase in mare basalts, lunar picritic glasses and the Mg-suite rocks (e.g., Longhi, 1992; Papike et al., 1998; Weitz et al., 1999; McCallum and Schwartz, 2001). This suggests that either spinel is a ubiquitous phase in the lunar mantle and that the melting relations producing these various rock types always resulted in spinel addition to the melt or that a common process such as anorthosite assimilation occurred to all of the lunar igneous magmas. With a globally distributed anorthite-rich crust it seems likely that at least some of the spinels observed in lunar magmas are the result of anorthosite assimilation.

5.4. Preservation of reacted melt

The physical and chemical properties of the melt modified by anorthosite dissolution will have important implications for dike propagation and melt flow through the lunar crust. Models of dike propagation (e.g., Lister and Kerr, 1991; Wilson and Head, 2003) utilize hydraulic fracture of the rock to accommodate dike formation. The hydraulic fracturing and physical properties of dikes produced will be a function of the magma density and viscosity. As shown in Fig. 9, anorthosite dissolution has a strong effect on both

the density and viscosity of the magma near the magma-wallrock interface. The physical and chemical properties of the thermo-chemical boundary layer are distinct from those of the reacting melt and must be included in order to model dike propagation through the lunar crust.

Melt-rock reaction occurs at magma-wallrock interface and hence is a local phenomenon. Given the highly turbulent nature of convective flow in large magma conduits, it is virtually impossible to prevent the reacted melt within the reactive boundary layer (δ_m in Fig. 1b) from mixing with the through-going picritic magmas, especially at greater depth. At shallower depths or near surface conditions where the distance over which the melts have left to travel before eruption is small, mixing between the reacted and unreacted melts may not be complete for two reasons: (1) the densities (viscosities) of the high-Al₂O₃ melts within δ_m are smaller (larger) than those of the unreacted picritic magmas, making them easier to separate or detach from the boundary layer; and (2) the segregated melts will have a better chance to preserve their chemical identity if the size of the magma conduit is small and the geometry of the conduit is not vertical, i.e., in a side branch of the main dike. Hence the volume of the partially preserved boundary layer melts is likely to be very small. In separate dike systems, the picritic magmas may originate from the relatively unmodified central region of a dike, away from the boundary layers along the walls of the dike. In contrast, the high-Al basalts may originate from within the chemically modified boundary layer near the edge of the dike. Chemically distinct magmas such as the picritic magmas and the high-Al basalts may result from different extents of crustal assimilation rather than differences in their source regions. More detailed studies are needed to further quantify this model.

6. Summary and conclusions

As pointed out by Finnila et al. (1994) both melting and dissolution may have played an important role in anorthosite assimilation during magma transport through the lunar crust. Although the driving forces for melting and dissolving are different (thermal vs. chemical, e.g., Woods, 1992), the chemical trends that developed during contact melting of the anorthositic crust are expected to be similar to those developed during anorthosite dissolution, at least within the thermal-chemical boundary layer. Hence the results from this study are also relevant to anorthosite assimilation via melting. The main conclusions of this study can be summarized as follows:

1. Lunar picritic magmas are strongly undersaturated with respect to anorthite. Consequently, anorthosite assimilation in the lunar picritic magmas is fast relative to that in terrestrial magmas.
2. Strong diffusive coupling is observed in lunar picritic magmas. The EBDC cannot adequately predict the diffusive behavior SiO₂ during magma-anorthosite interactions.

3. Diffusion-assisted assimilation results in nonlinear compositional profiles. The trend in increasing CaO and Al₂O₃ of the picritic glasses is consistent with modification of the magma by anorthosite assimilation.
4. Anorthosite assimilation in an olivine-saturated picritic magma may decrease the crystallinity of the reacting magma and lower its liquidus temperature.
5. The major element compositions of high-Al basalt may, in part, be the product of anorthosite assimilation into picritic glasses. If the parent magma for the high-Al basalts is chemically similar to the picritic magmas, then the high-Al basalts may be a product of anorthosite assimilation.
6. Anorthosite assimilation depends strongly on temperature, potentially resulting in spinel growth. The minor but ubiquitous observation of spinel in a variety of lunar volcanic and plutonic rocks may be an indication of anorthosite assimilation.
7. Dike propagation models through the lunar crust must consider anorthosite assimilation because the compositional effects on magma density, viscosity and crystallinity are significant.
8. More realistic models of anorthosite assimilation that include phase equilibria, thermal and chemical considerations of anorthosite–melt reaction are required in order to fully understand the role of anorthosite assimilation in lunar magma differentiation process.

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Appendix A. Diffusive dissolution in quaternary systems

The coupled one dimensional diffusion equations describing the distribution of a chemical species (i.e., C_i) in the melt in a four component system is given by (e.g., Zhang et al., 1989; Liang, 1999):

$$\frac{\partial C_1}{\partial t} = D_{11} \frac{\partial^2 C_1}{\partial x^2} + D_{12} \frac{\partial^2 C_2}{\partial x^2} + D_{13} \frac{\partial^2 C_3}{\partial x^2} + V \frac{\partial C_1}{\partial x}, \quad \text{for } x > 0, \quad (\text{A.1a})$$

$$\frac{\partial C_2}{\partial t} = D_{21} \frac{\partial^2 C_1}{\partial x^2} + D_{22} \frac{\partial^2 C_2}{\partial x^2} + D_{23} \frac{\partial^2 C_3}{\partial x^2} + V \frac{\partial C_2}{\partial x}, \quad \text{for } x > 0, \quad (\text{A.1b})$$

$$\frac{\partial C_3}{\partial t} = D_{31} \frac{\partial^2 C_1}{\partial x^2} + D_{32} \frac{\partial^2 C_2}{\partial x^2} + D_{33} \frac{\partial^2 C_3}{\partial x^2} + V \frac{\partial C_3}{\partial x}, \quad \text{for } x > 0, \quad (\text{A.1c})$$

where D_{ij} are the elements of the diffusion matrix with the 4th component as the dependent variable and V is the dissolution rate. Here the reference frame is centered on the moving solid–melt interface ($x = 0$). Following Liang (1999) we assume that the crystal and melt have the same density. The initial and boundary conditions are as follows:

$$C_1(x, 0) = C_{11}, C_2(x, 0) = C_{21}, C_3(x, 0) = C_{31}, \quad (\text{A.2a})$$

$$C_1(\infty, t) = C_{11}, C_2(\infty, t) = C_{21}, C_3(\infty, t) = C_{31}, \quad (\text{A.2b})$$

$$C_1(0, t) = C_{10}, C_2(0, t) = C_{20}, C_3(0, t) = C_{30}, \quad (\text{A.2c})$$

$$D_{11} \frac{\partial C_1}{\partial x} \Big|_{x=0} + D_{12} \frac{\partial C_2}{\partial x} \Big|_{x=0} + D_{13} \frac{\partial C_3}{\partial x} \Big|_{x=0} + V(C_{10} - C_{s1}) = 0, \quad (\text{A.2d})$$

$$D_{21} \frac{\partial C_1}{\partial x} \Big|_{x=0} + D_{22} \frac{\partial C_2}{\partial x} \Big|_{x=0} + D_{23} \frac{\partial C_3}{\partial x} \Big|_{x=0} + V(C_{20} - C_{s2}) = 0, \quad (\text{A.2e})$$

$$D_{31} \frac{\partial C_1}{\partial x} \Big|_{x=0} + D_{32} \frac{\partial C_2}{\partial x} \Big|_{x=0} + D_{33} \frac{\partial C_3}{\partial x} \Big|_{x=0} + V(C_{30} - C_{s3}) = 0, \quad (\text{A.2f})$$

where C_{si} are the concentration of i in the solid and C_{i0} are the concentration of the melt at the interface with the solid. To simplify our calculations we estimate the diffusion matrix by assuming that the diffusive fluxes of CaO and FeO are not coupled to the concentration gradients of the higher charge species (TiO₂, Al₂O₃, and SiO₂) and that the higher charge species do not couple with each other. This limits the number equations we need to solve to an effective quaternary system. Additionally, if we assume components 1 and 2 are the uncoupled CaO and FeO, then it minimizes the number of diffusion terms in Eqs. A1 and A2 (i.e., D_{12} , D_{13} and D_{21} and D_{23} are equal to 0). The exact solution to the quaternary system directly follows the ternary solution of Liang (1999), viz.,

$$C_1 = C_{11} + (C_{10} - C_{11})E_1, \quad (\text{A.3a})$$

$$C_2 = C_{21} + (C_{20} - C_{21})E_2, \quad (\text{A.3b})$$

$$C_3 = C_{31} - \left[\frac{D_{31}(C_{10} - C_{11})}{D_{33} - D_{11}} \right] E_1 - \left[\frac{D_{32}(C_{20} - C_{21})}{D_{33} - D_{22}} \right] E_2 + \left\{ (C_{30} - C_{31}) + \left[\frac{D_{31}(C_{10} - C_{11})}{D_{33} - D_{11}} \right] + \left[\frac{D_{32}(C_{20} - C_{21})}{D_{33} - D_{22}} \right] \right\} E_3, \quad (\text{A.3c})$$

where α is a dimensionless dissolution parameter; E_1 , E_2 , and E_3 are defined as

$$E_i = \operatorname{erfc} \left(\frac{x}{2\sqrt{D_{ii}t}} + \alpha \sqrt{\frac{D_{11}}{D_{ii}}} \right) \left[\operatorname{erfc} \left(\alpha \sqrt{\frac{D_{11}}{D_{ii}}} \right) \right]^{-1}, \quad \text{for } i = 1, 2, 3. \quad (\text{A.4})$$

The dissolution rate, V , and the dissolution distance X_b are given by

$$V = \alpha \sqrt{\frac{D_{11}}{t}}, \quad (\text{A.5})$$

$$X_b = 2\alpha \sqrt{D_{11}t}. \quad (\text{A.6})$$

In contrast to Liang (1999) we use our independently measured dissolution distances (Fig. 4 and Table 2) and Eqs. (A.5) or (A.6) to calculate the α parameter.

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