



ELSEVIER

Available online at www.sciencedirect.com

SCIENCE @ DIRECT®

Journal of Applied Geophysics 54 (2003) 411–425

JOURNAL OF
APPLIED
GEOPHYSICS

www.elsevier.com/locate/jappgeo

Anisotropic viscoelastic models with singular memory

A. Hanyga

Institute of Solid Earth Physics, University of Bergen, Allégaten 41, N5007 Bergen, Norway

Abstract

The physical background of singular memory models and in particular the Cole–Cole model is discussed. Three models of anisotropic linear viscoelasticity with frequency-dependent stiffness coefficients are considered. The models are constructed in such a way that anisotropic properties are separated from anelastic effects. Two of these models represent finite-speed wave propagation with singularities at the wavefronts (the exponential relaxation model) and without singularities at the wavefronts (the Cole–Cole model), while a third model called the fractional model is related to the constant Q with unbounded propagation speed. The Cole–Cole and fractional models belong to the class of singular memory models studied earlier because of their applications in polymer rheology, poroelasticity, poroacoustics, seismic wave propagation and other applications. Well-posedness of initial boundary value problems with mixed Dirichlet–Neumann boundary conditions is established for the three models. Regularity properties of the three models are examined.

© 2003 Elsevier B.V. All rights reserved.

Keywords: Viscoelasticity; Anisotropy; Attenuation

1. Introduction

The Cole–Cole hereditary law has been very successful in modeling dispersive properties of dielectrics (Cole and Cole, 1941) and anelastic mechanical response in polymers, where it is known by the name of Bagley–Torvik (Bagley and Torvik, 1986). It allows a very accurate modeling of the frequency dependence of the dielectric constant or the anelastic moduli over a very large range of frequencies provided the material exhibits only a single transition region between the low-frequency and the high-frequency regime (and a single minimum of the Q parameter) (Soula and Chevalier, 1998). It is known from alternative models of the same response function that a comparable result based on rational functions requires polynomials of fifth degree (Soula et al., 1997). It therefore comes as

no surprise that the Cole–Cole model has recently been found to allow a very good matching for the observed dispersive properties of elastic moduli in rocks (Batzle et al., 2001). In a related context of dielectric properties of porous media it appears in Ruffet et al. (1991) and Taherian et al. (1990). The Cole–Cole model has a potential for adding new features, such as additional transition zones in the spectral response function, by including additional fractional powers of frequency in the numerator and denominator (Torvik and Bagley, 1983; Fenander, 1997). Dispersion in rocks, mostly due to the fluid saturation, generally exhibits a single transition zone and a single peak of the inverse quality factor (e.g., Tutuncu et al., 1998). The Cole–Cole model in its simplest form is adequate for this case.

The Cole–Cole model is a member of a class of models which are defined in terms of “springpots” (Koeller, 1984), which constitute an intermediate ob-

E-mail address: andrzej@ifjf.uib.no (A. Hanyga).

ject between a spring and a dashpot, in the way of Maxwell–Voigt–Zener models. The springpots are parameterized by their order, contained between 0 and 1, with 0 corresponding to the spring and 1 corresponding to the dashpot. A Kelvin–Voigt element with a springpot replacing the dashpot is often used as a model of a viscous oscillation damper (for an extensive bibliography on this subject and other engineering applications, see Agrawal (1999); Rossikhin and Shitikova, 1997). Since springpots can have different orders, this class of models is much richer than the Maxwell–Voigt class. For example replacing a single dashpot by two springpots of different order connected in parallel (Rossikhin and Shitikova, 2001) yields a new model of viscous response. In this context the Cole–Cole relaxation is a generalized Standard Linear Solid with the dashpots replaced by springpots of the same order.

The Cole–Cole model belongs to the category of singular memory models, i.e., hereditary models with the constitutive relations represented by weakly singular convolution kernels. The first singular memory model of viscous behavior was due to Boltzmann (Boltzmann, 1876). It involved the Hilbert kernel $(t - \tau)^{-1}$. It is nowadays known that such a strong (nonintegrable) singularity results in an infinite speed of propagation (Renardy, 1982).

In hereditary viscoelasticity the stress is given by the constitutive law $\sigma(t) = G(0)e(t) + G'(t)*e(t)$. In general, $G(0) > 0$ ensures a finite propagation speed. Singular memory is defined by the asymptotic property $G'(t) \sim \text{const} \times t^{-\gamma} + \dots$ for $t \rightarrow 0$, $0 < \gamma < 1$, of the kernel. Note that $G(t)$ is the stress relaxation function (stress response to a jump of strain from zero to a constant level at one). The singularity of the delayed response kernel $G'(t)$ gives much more weight to the very recent past of the strain history than to the rest of it.

The Cole–Cole model can also be represented in terms of a relaxation equation for stress and strain involving fractional derivatives (Podlubny, 1998; Miller and Ross, 1993). More general relaxation laws involving fractional derivatives have been discussed by Bagley and Torvik (1983c), Torvik and Bagley (1984) and Fenander (1997). Relaxation models based on fractional derivatives originated in the theory developed by Gemant (1936, 1938) and Blair (1944). The theory of Gemant and Scott Blair was in turn stimulated by the papers of Nutting on generic creep laws (Nut-

ting, 1921, 1943, 1946), who pointed out that the experimental creep laws of that time could be expressed by a simple relation between the strain, stress and time $\epsilon \sim \sigma^\alpha t^\beta$, with $\alpha > 0$ accounting for nonlinearity and $0 < \beta \leq 1$ indicating that a fractional derivative of order < 1 may be involved. In Russian literature two classes of weakly singular kernels related to the Cole–Cole law, the Rabotnov kernel (Rabotnov, 1969, 1980) and the Rzhantsyn kernel (Rzhantsyn, 1949, 1968; Rossikhin and Shitikova, 1997), are widely used. Applications of fractional derivatives in phenomenological polymer rheology and in disordered systems have a long and rich history (Bronskii, 1941; Slonimsky, 1939, 1961, 1967; Havriliak and Negami, 1967; Nigmatullin, 1984, 1986; Friedrich, 1991; Friedrich and Braun, 1992; Bagley and Torvik, 1983a, 1986; Torvik and Bagley, 1983; Glöckle and Nonnenmacher, 1991, 1994; Schiessel and Blumen, 1993; Heymans and Bauwens, 1994; Rogers, 1983; Eldred et al., 1995; Palade et al., 1996), to mention but a few representative papers. Another material often reported in this connection was rubber, for which a simple viscous memory kernel $(t - \tau)^{-\gamma}$, $0 < \gamma < 1$, was suggested by Duffing (1931). De Andrade's law for creep in metals also falls in this category (Andrade, 1910, 1912).

Power laws of attenuation in acoustics (Szabo, 1994, 1995; Szabo and Wu, 2000) and in seismology (Strick, 1984) can be expressed in terms of fractional derivatives. The corresponding theoretical models are discussed in Hanyga and Sereďynska (1999a, 2002), Hanyga and Rok (2000) and in some earlier papers referenced there. More recently, evidence for the validity of power law has come from inversion of laboratory data and marine seismic data (Ribodetti and Hanyga, 2004). Although power laws can be considered as a high-frequency approximation of the Cole–Cole model, they do not satisfy the requirements of the theory developed in this paper in the anisotropic case.

In engineering, fractional models of viscoelastic relaxation were applied among others by Enelund et al. (1997), Enelund and Josefson (1997), Enelund and Lesieutre (1999), Enelund and Olsson (1998), Bagley (1990), Bagley and Torvik (1983b), Torvik and Bagley (1985) Bagley and Calico (1991) and Schmidt et al. (2000). In the general context of viscous mechanical damping of structural elements in particular the references Suarez and Shokooh (1995, 1997), Beyer and Kempfle (1995), Gaul et al. (1989, 1991), Mbdje

et al. (1994) and Sereďyńska and Hanyga (2000) make use of fractional derivatives. In rock mechanics the Cole–Cole elastic modulus was discussed by Jones (1986). Additional references can be found in Podlubny (1998) and Rossikhin and Shitikova (1997).

One of the first applications of fractional calculus in viscoelasticity was, however, seismic attenuation (Caputo and Mainardi, 1971, 1976; Caputo, 1969), in particular the Caputo–Kjartansson constant Q model (Caputo, 1967a,b; Mainardi and Tomirotti, 1997; Hanyga, 2002b; Carcione et al., 2002; Kjartansson, 1979). In the same context the Cole–Cole model was discussed and compared with the Caputo–Kjartansson model by Jones (1986). In a scalar model of wave propagation, the constant Q can be modeled by a Cole–Cole law with a low value of the exponent (Hanyga, 2003a). Unlike the Caputo–Kjartansson model, the Cole–Cole model is compatible with the requirement of finite propagation speed. In rock mechanics dispersion and attenuation is essentially due to pore fluid flow (Tutuncu et al., 1998) and can thus be accounted for by poroelastic models. Fast-to-slow wave conversion (Gurevich and Lopatnikov, 1997; Hanyga and Rok, 2000), squirt flow (Dvorkin and Nur, 1993) and patchy fluid saturation (Johnson, 2001) can be expected to generate singular memory effects in the seismic frequency range. Biot's theory also involves a weakly singular kernel associated with the dynamic permeability (Hanyga, 1999a, 2001c). In Biot's poroelasticity, singular memory effects are expected to be observable above the Biot frequency, i.e., in the acoustic log and ultrasound frequency ranges. For rigid air-saturated materials, both the permeability and bulk modulus are represented by singular memory kernels (an extensive bibliography and mathematical analysis can be found in Hanyga (2001b)).

Poroelasticity (e.g., Norris, 1986; Berryman et al., 1988) and poroacoustics (e.g., Wilson, 1992; Allard and Champoux, 1992; Stinson and Champoux, 1992) involve singular memory kernels of a more complicated type. Singular memory models of anelastic mechanical response constitute a much larger class than fractional derivative models. In wave propagation, modeling the former can often be replaced by the latter. Asymptotic analysis of wave propagation shows that the singular part of the memory kernel plays a predominant role in shaping the signal of the wavefront region, while the regular part of the memory merely accounts

for an additional amplitude decay and can often be replaced by a constant (Hanyga and Sereďyńska, 1999a, 2002). Consequently, relaxation models involving singular kernels can be simplified by introducing simple fractional relaxation laws with the regular part of the memory kernel replaced by a constant.

In scalar hyperbolic problems the memory effects are represented by invertible convolution operators. Assuming a homogeneous medium memory, operators can be flipped from the spatial derivative operator to the inertial terms (time derivatives) and vice versa. Applying the simplification described in the previous paragraph to an equation in which the memory appears in the inertial term, one obtains a solution which represents a generalized power law of attenuation (possibly with several power terms involving different exponents; Hanyga and Sereďyńska, 2002). An equivalent equation with the memory operator acting on the space derivatives is more complicated and involves generalized Mittag–Leffler functions (Engler, 1997). Such equations have some explicit solutions Hanyga and Sereďyńska (1999a, 2002) that can be studied in much detail. Unfortunately, these special models have some undesirable features, e.g., an unbounded creep function (Engler, 1997). It can, however, be shown that the power law behavior is a universal feature of asymptotic solutions for singular memory models, i.e., it is a general feature of the spectrum of the signal following a wavefront (Hanyga and Sereďyńska, 1999a, 2002).

The Cole–Cole relaxation model has many advantages over the other models. It is compatible with a finite speed of propagation. It essentially involves only the singular response and therefore can be represented by fractional derivatives. The Cole–Cole modulus has the same form whether applied to the inertial term or to the spatial term in the equation. The Cole–Cole creep function is bounded and tends to the inverse relaxed modulus for $t \rightarrow \infty$. Constant Q can be simulated by a Cole–Cole model with a low value of the exponent (Hanyga, 2003a).

In a hyperbolic model the speed of propagation is bounded by its infinite frequency limit. The solution vanishes outside a region bounded by a wavefront. Singular memory entails smoothing at the wavefronts, as shown in various contexts in (Narain and Joseph, 1982; Renardy, 1982; Hrusa and Renardy, 1988; Desch and Grimmer, 1986, 1989a,b; Prüss, 1993; Hanyga, 2001b). Combination of finite wave propagation speed

with smoothing results in a signal delay with respect to the wavefront (Hanyga and Sereďyńska, 1999b; Hanyga and Rok, 2000). These effects were studied in much detail in the case of scalar hyperbolic equations with singular memory (Lokshin and Rok, 1978a,b; Hanyga and Rok, 2000; Hanyga, 2001b; Hanyga and Sereďyńska, 2002), where explicit solutions can be often constructed. The solutions of such scalar hyperbolic equations largely overlap with phenomenological power-frequency models of acoustic attenuation (Szabo, 1994, 1995; Szabo and Wu, 2000; Strick, 1984). Simple attenuation models such as power laws or constant Q can only be obtained in the context of scalar equations. Since simplicity is lost in anisotropic models, flexibility of the Cole–Cole and related models becomes a more important asset.

For nonlinear viscoelastic problems with $G(0) > 0$ (i.e., with a bounded propagation speed) and with singular memory, smoothing does not extend to shock waves, which propagate as discontinuities (Gripenberg, 2001).

Smoothing in a hyperbolic model entails an additional effect: signal delay with respect to the wavefront. The wavefront is the boundary between the undisturbed medium and the wavefield. Its speed of propagation is equal to the infinite frequency limit of the frequency-dependent propagation speed. A smooth peaked signal must lag behind the wavefront because the only peaked signals that can propagate with the wavefront are the Dirac delta and its derivatives. The resulting signal delay for a source delta-spiked signal can be calculated (Hanyga and Sereďyńska, 1999b, 2002).

In this paper the Cole–Cole stress relaxation law will be incorporated in the constitutive relations of anisotropic elasticity following a method of Carcione and Cavallini (1994) and Carcione et al. (1996). The method of Carcione and Cavallini (1994) and Carcione et al. (1996) is based on an a priori constraint on the constitutive equations which restricts the frequency dependence to the eigenvalues of the stiffness tensor. Directional dependence of anelastic medium parameters is represented by frequency-independent eigenstrain tensors. The material symmetry of the medium and the directional dependence of anelastic moduli are thus decoupled from the frequency-dependent scalar parameters. Such an assumption may be inconsistent with physical models derived by averaging, homoge-

nization or physical models (Gurevich, priv. comm). In the absence of a physical model it is, however, a convenient tool for restricting the number of model parameters and ensuring causality. In seismology, information about the anisotropic features of the medium is obtained on the assumption that the medium is elastic. It is therefore convenient to preserve this information while introducing viscous effects. The decomposition of stiffness matrix in terms of eigenstrains and scalar stress relaxation kernels is, however, not necessary for the well-posedness and regularity, as shown in Hanyga (2003c).

Regularity and well-posedness results obtained so far apply to some special classes of equations (one-dimensional viscoelasticity and poroacoustics (Hanyga, 2001b), or anelastic models with a single relaxation mechanism (Prüss, 1993; Desch and Grimmer, 1986)). In particular, existence, uniqueness and regularity results for three-dimensional anelastic models with several different relaxation functions controlling the stress response have not been obtained previously. We present here the uniqueness, existence and regularity results obtained recently in Hanyga (2003c), skipping mathematical details and focusing on the Cole–Cole relaxation model and on two qualitatively different relaxation models, viz., the exponential relaxation and the fractional relaxation.

It should be emphasised that in hereditary viscoelasticity the issue of existence and uniqueness is far from trivial and depends on such properties of the memory kernels as positivity, monotonicity and convexity (Hrusa and Renardy, 1988; Desch and Grimmer, 1989a,b; Prüss, 1993). For the kernels considered in this paper a stronger property (complete monotonicity) was more convenient in proofs of existence and uniqueness. Regularity of solutions and finite propagation speed depend on additional properties of these kernels (Section 5). As mentioned above, finite propagation speed in combination with smoothness implies signal delay. In the context of the relaxation models discussed in this paper only the Cole–Cole relaxation has both features. Relevance of signal delay for inversion is demonstrated in Hanyga and Sereďyńska (1999b).

Numerical methods for solving basic initial-value problems for the viscoelastic media with the Cole–Cole relaxation kernel and other singular memory kernels are discussed in Rossikhin and Shitikova (2000) and Hanyga (2002a). They are based on a

reformulation of the problem in terms of fractional derivatives and an adequate discretization. Time-stepping schemes for fractional time derivatives have been developed (Hanyga, 1999b,c) and implemented (Carcione et al., 2002) in a scalar model of constant Q due to Caputo and Mainardi (Caputo, 1967a; Mainardi and Tomirotti, 1997). The earliest algorithms for fractional time-stepping in structural mechanics are due to Padovan (1987) (with FEM), Koh and Kelly (1990) and Makris et al. (1993) (with BEM). Alternatively, it is possible to express the problem in terms of partial differential equations with additional variables satisfying fractional relaxation equations (Hanyga, 2003b). Important applications in polymer rheology have led to a recent spate of numerical schemes for ordinary differential equations of fractional order designed for applications in viscoelastic and viscoplastic models (the references Diethelm et al. (2002) and Diethelm and Freed (1999) are most relevant for the equations considered in Hanyga (2003b)). It is also possible to eliminate fractional derivatives by introducing an auxiliary variable satisfying an integrodifferential equation (Mbodje et al., 1994; Yuan and Agrawal, 1998). General multistep schemes of an arbitrary order of accuracy can be derived from Lubich’s quadratures and numerical schemes for Volterra equations (Lubich, 1986, 1988a,b; Brunner and van der Houwen, 1986).

2. The Cole–Cole response

The Cole–Cole transfer function can be expressed in the following form

$$\hat{M}(\omega) = M_\infty \frac{1 + a(-i\omega\tau)^{-\alpha}}{1 + (-i\omega\tau)^{-\alpha}} \quad (1)$$

where $\hat{M}(\omega)$ stands for some frequency-dependent modulus (e.g., Young’s modulus in Bagley and Torvik’s polymer model), M_∞ denotes the high-frequency limit of $\hat{M}(\omega)$, τ represents a characteristic relaxation time and $0 < \alpha < 1$. Thermodynamic arguments (Bagley and Torvik, 1986) imply that the exponent α in the numerator and in the denominator are equal. Furthermore, the relaxed modulus $M_0 = aM_\infty$ cannot exceed the instantaneous modulus M_∞ , hence $a < 1$. This inequality follows from thermodynamics (Fabrizio and Morro, 1992; Bagley and Torvik, 1986) and is

known from creep tests. The exponent α controls the width of the transition zone between M_0 and M_∞ .

The asymptotic behavior of the Cole–Cole transfer function for $\omega \rightarrow \infty$

$$\hat{M}(\omega) \sim M_\infty [1 + (a - 1)(-i\omega\tau)^{-\alpha}] \quad (2)$$

The first term corresponds to an immediate elastic response. The delayed response is dominated by a power law, which is a well-known universal law for relaxations, including mechanical relaxation (Jonscher, 1996). Universality of this feature has prompted many scientists to develop a statistical model of relaxation based on direct statistical arguments (Weron and Kotulski, 1996) or on anomalous diffusion, more specifically, on the continuous time random walk model of anomalous diffusion (Gomi and Yonezawa, 1995). The relaxation of the modes of the associated fractional Fokker–Planck equation turns out to obey the Cole–Cole law (sometimes referred to as the Mittag–Leffler law) (Metzler et al., 1999). An important feature of these theoretical models is universality due to a very fundamental and generic physical micromodel.

In time domain the Cole–Cole response is expressed in terms of a time convolution. Let $E_{\gamma,\beta}(z)$ denote the generalized Mittag–Leffler function (Podlubny, 1998)

$$E_{\gamma,\beta}(z) := \sum_{n=0}^{\infty} \frac{z^n}{\Gamma(\gamma n + \beta)} \quad (3)$$

for arbitrary complex z . The Mittag–Leffler function proper $E_\gamma(z) := E_{\gamma,1}(z)$ is a special case of the generalized Mittag–Leffler function.

The stress relaxation function of the Cole–Cole model is

$$R(t) = M_0 + (M_\infty - M_0)E_\alpha(-(t/\tau)^\alpha) \quad (4)$$

(Fig. 1) (Hanyga, 2002a).

For a strain $e(t)$ such that $t^z e(t) \rightarrow 0$ for $t \rightarrow 1$ and e is right-continuous at 0, the stress is given by inverse Fourier transform of $\hat{M}(\omega) \hat{f}(\omega)$

$$\sigma(t) = M_\infty e(t) + (1 - a)M_\infty \times \int_0^\infty E_\alpha(-(\theta/\tau)^\alpha) e'(t - \theta) d\theta \quad (5)$$

in the time domain.

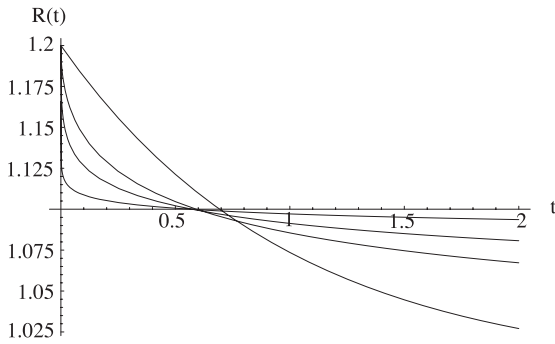


Fig. 1. The Cole–Cole relaxation function $R(t)$ for $\alpha = 0.5, 0.3, 0.1$ compared with exponential relaxation $R_{\text{exp}}(t) = M_{\infty} + (M_0 - M_{\infty}) \exp(-t/\tau)$. The Cole–Cole relaxation function has an infinite slope at $t = 0$. Smaller values of α correspond to higher initial slope and longer tails. $M_0 = 1, M_{\infty} = 0.8 M_0$.

The Laplace transform \tilde{K} of the corresponding compliance $K(t)$ is given by the equation $\tilde{R}(s) \tilde{K}(s) = 1/s$, hence

$$\tilde{K}(s) = M_{\infty}^{-1} \frac{1 + a^{-1}(s\tau')^{-\alpha}}{1 + (s\tau')^{-\alpha}}$$

where $\tau' := a^{-1/\alpha}\tau$. The creep function $J(t)$, i.e., the strain response to a unit step stress jump, is the inverse Laplace transform of $s^{-1} \tilde{K}(s)$, hence $J(t) = M_{\infty}^{-1} + (M_0^{-1} - M_{\infty}^{-1})E_{\alpha}(- (t/\tau')^{\alpha})$ (Fig. 2).

The corresponding strain rate has the singularity $M_{\infty}^{-1}(a^{-1} - 1)\tau'^{-1} (t/\tau')^{\alpha-1}$, which implies that the initial creep rate is infinite, a well-known fact in experimental mechanics (cf. e.g., Kohlrausch, 1847, 1863; Nutting, 1946; Rabotnov, 1969; Rossikhin and Shitikova, 1997).¹ Attempts to incorporate this feature in the stress relaxation function (or its counterpart the dielectric decay function) has led to the stretched exponential a.k.a. Kohlrausch–Watts–Williams

¹ In a hyperbolic model of viscoelasticity the creep function $J(\tau)$ and the stress relaxation function $G(\tau)$ have identical singularities. Indeed, the relations $\sigma = G * e'$ and $e = J * \sigma'$ imply that their Laplace transforms satisfy the relation $\tilde{J}(s) \tilde{G}(s) = s^{-2}$. For a singular memory hyperbolic model with $G(t) = G(0)H(t) - at^{\alpha}/\Gamma(\alpha+1) + \dots$, $0 < \alpha < 1$, where $H(t)$ denotes the unit step function, an Abelian theorem implies that $\tilde{G}(s) \sim G(0) s^{-1} - a s^{-\alpha-1} + \dots$ for $s \rightarrow \infty$, whence $\tilde{J}(s) \sim G(0)^{-1} s^{-1} + [a/G(0)^2] s^{-\alpha-1}$ in the same limit. In view of the positivity and monotonicity property a Karamata Tauberian theorem (Widder, 1946) implies that $J(t) = G(0)^{-1} H(t) + [a/G(0)^2] t^{\alpha}/\Gamma(\alpha+1) + \dots$ for small t .

(KWW) law $G(t) = M \exp(- (t/\tau)^{\alpha})$, $0 < \alpha < 1$ (see Williams and Watts, 1970). The stretched exponential is an empirical law with a rather complicated frequency domain counterpart (Williams and Watts, 1970). The Cole–Cole response has the same short-time asymptotics as the (KWW) law and a simple algebraic frequency-domain form, convenient for parameter estimation. The two differ in the long time range: in contrast to the KWW law, the Cole–Cole response has a fat tail (an algebraic decay rate at infinity). The last feature has little relevance for wave propagation but there is an experimental evidence for it in polymer rheology (Klafter et al., 1986).

Unlike some other fractional derivative models, the Cole–Cole relaxation model is characterized by a bounded creep function $J(t)$. In fact

$$\tilde{J}(s) = \frac{1}{M_0 s} \frac{1 + (\tau s)^{\alpha}}{a + (\tau s)^{\alpha}} \sim \frac{1}{asM_0} [1 - (a^{-1} - 1)(\tau s)^{\alpha}]$$

for small s . Hence, taking into account the nonnegativity and monotonicity of the creep function, we have by a Tauberian theorem

$$J(t) \sim \frac{1}{M_{\infty}} [1 - (a^{-1} - 1)(t/\tau)^{-\alpha}]$$

tends to $1/M_{\infty}$ for $t \rightarrow \infty$.

The Cole–Cole response has some statistical justification (Gomi and Yonezawa, 1995; Weron and Kotulski, 1996) of a rather universal nature.

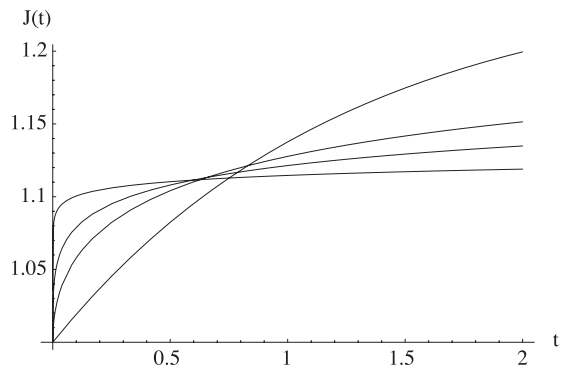


Fig. 2. The corresponding creep functions $J(t)$. Lower values of α correspond to higher initial strain rate and slower final strain rate.

3. The anisotropic Cole–Cole model

The elastic stiffness tensor c_{klmn} can be considered as a 6×6 positive semidefinite symmetric matrix C_{rs} . The matrix C_{rs} can be decomposed in terms of dyadics $v_r^{(p)} v_s^{(p)}$, where $v^{(p)}$ denote the unit eigenvectors of C_{rs} . Reverting to tensor notation for the three-dimensional space

$$c_{klmn} = \sum_{p=1}^6 A_p^0 e_{kl}^{(p)} e_{mn}^{(p)} \quad (6)$$

where $A_p^0, p = 1, \dots, 6$, are the eigenvalues of C_{rs} and the eigenstrains $e_{kl}^{(p)}$ are the eigenvectors $v_r^{(p)}$ expressed in 3×3 tensor notation. They are assumed orthonormal in the sense of

$$e_{kl}^{(p)} e_{kl}^{(q)} = \delta_{pq} \quad (7)$$

(Helbig, 1994). An eigenstrain is defined by the property that the corresponding stress differs from it by a scalar factor A . We shall use the shorthand notation $E = \{e_{kl}\}$, $E^{(p)} = \{e_{kl}^{(p)}\}$, $\langle E, E' \rangle = e_{kl} e'_{kl}$, $C[E] = \{g_{klmn} e_{mn}\}$ and $C = \sum_p A_p^0 E^{(p)} \otimes E^{(p)}$ and fixed, frequency-independent material symmetry properties.

We shall now construct a viscoelastic memory kernel $G(t)$ with the elastic part $G(0) = C$. Let \mathcal{G} denote the material symmetry group of the elastic medium defined by the stiffness tensor C . For a solid in a nondeformed configuration (Truesdell, 1972) $\mathcal{G} \subset SO(3)$ and the property $Q \in \mathcal{G}$ is equivalent to $C[\hat{Q}[E]] = \hat{Q}[C[E]]$ for every symmetric tensor E , where $\hat{Q}[E] := QEQ^T$ is a rotation in the six-dimensional space of symmetric tensors E , and

$$C[E] := \sum_{p=1}^6 A_p^0 \langle E, E^{(p)} \rangle E^{(p)} \quad (8)$$

The eigenvalues A_p^0 can be divided into groups in such a way that A_p^0 and A_r^0 are equal if and only if they belong to the same group. We now associate the parameters $a_p, \alpha_p, \tau_p, 0 < \alpha_p < 1, 0 \leq a_p \leq 1, \tau_p > 0$, with each group of eigenvalues and define

$$A_p(-i\omega) := A_p^0 \frac{1 + a_p(-i\omega\tau_p)^{-\alpha_p}}{1 + (-i\omega\tau_p)^{-\alpha_p}} \quad (9)$$

The tensor-valued anelastic stress relaxation function is now given by the formula

$$\hat{G}(\omega) = \sum_p (-i\omega)^{-1} A_p(-i\omega) E^{(p)} \otimes E^{(p)} \quad (10)$$

or, in the time domain,

$$G(t) = \sum_p r_p(t) E^{(p)} \otimes E^{(p)} \quad (11)$$

where $r_p(t)$ denotes the inverse Laplace transform of $A_p(s)/s$. The corresponding stress–strain response function $\lambda_p(t) = r_p'(t)$ is given by Eq. (5). According to Theorem 2 in Appendix 2 of Hanyga (2002a), every $Q \in \mathcal{G}$ is a material symmetry of $\hat{G}(\omega)$ and vice versa, i.e., $\hat{G}(\omega)$ and C have the same material symmetry for every ω . Thermodynamic restrictions on G (Fabrizio and Morro, 1992) are satisfied in view of the inequality $a_p \leq 1$ in combination with the major symmetry of $G_{klmn}(t)$.

For comparison we shall also discuss the exponential relaxation and the fractional relaxation model:

$$A_p(s) = a_p + \sum_{n=1}^N b_p^{(n)} / (s + 1/\tau_p^{(n)});$$

$$\lambda_p(t) = a_p \delta(t) + \sum_{n=1}^N b_p^{(n)} e^{-t/\tau_p^{(n)}} \quad (12)$$

$$A_p(s) = a_p s^{\alpha_p}; \quad \lambda_p(t) = a_p t^{-\alpha_p - 1} / \Gamma(-\alpha_p) \quad (13)$$

with $a_p > b_p \geq 0$ in the first case and $a_p > 0$ in the second case. The last inequality in combination with the major symmetry of the tensor-valued function G ensures that the thermodynamic restrictions are satisfied (Fabrizio and Morro, 1992).

4. Energy dissipation

In the absence of thermal effects the condition of nonnegative dissipation usually takes the form

$$\psi' \leq \langle \sigma, e' \rangle$$

where ψ is some sort of energy. Unfortunately, the energy is not uniquely defined in a hereditary medium and, consequently, it is convenient to consider energy

dissipation on a cycle (or on a quasi-cycle, since cycles consistent with the equations of motion may not exist in a sufficient number):

$$\oint \langle \sigma(t), e'(t) \rangle dt \equiv \int_0^T \langle \sigma(t), e'(t) \rangle dt \geq 0 \quad (14)$$

for periodic $e(t)$ with a period T (in this case $\sigma(t)$ is clearly periodic too). Inequality (14) entails the inequalities $G_\infty := \lim_{t \rightarrow \infty} G(t) \geq 0$ and Graffi's inequality

$$\int_0^\infty G(t) \sin(\omega t) dt < 0 \quad \text{for } \omega > 0$$

As shown in Fabrizio and Morro (1992), this in turn implies that

$$\int_{-\infty}^t \langle \sigma(\tau), e'(\tau) \rangle d\tau \geq 0 \quad (15)$$

for arbitrary square integrable $e(t)$ having square integrable derivatives.

Obviously, Eq. (15) entails Eq. (14) as a particular case. This provides us with a criterion of thermodynamic dissipativity.

We shall now show that Eq. (15) is satisfied in virtue of our assumptions in the previous section.

Let e be a constant symmetric matrix. Since

$$\langle e, G(t)e \rangle = \sum_p r_p(t) \langle e, E^{(p)} \rangle^2$$

the derivatives of $G(t)$ satisfy the inequalities

$$(-1)^n \langle e, G^{(n)}(t)e \rangle \geq 0 \quad n = 0, 1, 2, \dots \quad (16)$$

for $t > 0$. In the terminology of Gripenberg et al. (1990), $G(t)$ is a completely monotonic matrix function on $t > 0$ and, consequently, it is infinitely differentiable for $t > 0$. In particular, Eq. (16) restricted to $n = 0, 1, 2$ implies that $G(t)$ is a matrix function of positive type (Gripenberg et al., 1990; Yosida, 1974), whence

$$\int_{-\infty}^\infty \int_{-\infty}^\infty \langle \varepsilon(t), G(t - \tau)\varepsilon(\tau) \rangle dt d\tau \geq 0 \quad (17)$$

for arbitrary square integrable functions $\varepsilon(t)$ with values in the space of symmetric matrices. Taking in particular

$$\varepsilon(t) = \begin{cases} e'(t), & t < T \\ 0 & t > T \end{cases}$$

for an arbitrary $T > 0$, we have, in view of causality,

$$\int_{-\infty}^T dt \int_{-\infty}^t \langle e'(t), G(t - \tau)e'(\tau) \rangle d\tau \equiv \int_{-\infty}^T \langle \sigma(t), e'(t) \rangle dt \geq 0$$

hence, Eq. (15) is satisfied on account of $(-1)^n r_p^{(n)}(t) \geq 0$ for $t > 0$ and $n = 0, 1, 2$.

This explains the role of monotonicity and convexity of memory functions in hereditary viscoelasticity.

5. Well-posedness

In view of their complicated form integrodifferential equations require a verification of the well-posedness of the associated initial-boundary value problems. The existence and uniqueness of solutions depend on the monotonicity and convexity of the memory kernel.

The initial-boundary value problem for the equations of motion will be formulated along the lines of Desch and Grimmer (1989a). Let Ω be a bounded domain in \mathbb{R}^3 with a C^2 -smooth boundary $\partial\Omega = \Gamma_1 \cup \Gamma_2$, where $\Gamma_1 \cap \Gamma_2 = \emptyset$. Let n_k denote the unit exterior normal on Γ_2 . We shall consider the boundary-value problem on $\mathbb{R} \times \Omega$

$$\rho \dot{v}_k = \sigma_{kl,l} \quad \text{for } k = 1, 2, 3 \quad (18)$$

$$\sigma_{kl} = g_{klmn} * v_{m,n} \quad (19)$$

$$v_k(t, \mathbf{x}) = 0, \quad k = 1, 2, 3 \quad \text{on } \Gamma_1$$

$$\sigma_{kl}(t, \mathbf{x})n_l = 0, \quad k = 1, 2, 3 \quad \text{on } \Gamma_2 \quad (20)$$

with initial data derived from an initial history $v_k^{(0)}(t, \mathbf{x})$, $k = 1, 2, 3$, $t \leq 0$, of the velocity field.

For the proof of well-posedness the key property of the matrix-valued memory kernel G is complete monotonicity, defined here by the equation

$$G(t) = \int_0^\infty e^{-t\zeta} dF(\zeta), \quad t > 0 \tag{21}$$

where $F = \{f_{klmn}\}_{k,l,m,n=1,2,3}$ is a tensor-valued function on $\overline{\mathbb{R}_+}$ with the symmetries of g_{klmn}

$$F(\zeta) = \sum_{p=1}^P \mu_p(\zeta) G^{(p)} \tag{22}$$

$\mu_p, p=1, \dots, P$, are nondecreasing functions with bounded variation, the integral is interpreted as a Laplace–Stieltjes integral and the tensors $G^{(p)}$ are positive in the sense

$$g_{klmn}^{(p)} \zeta_{kl} \zeta_{mn} \geq 0 \quad \forall \zeta \in \mathcal{S} \tag{23}$$

In a heterogeneous medium the tensor-valued function G_{klmn} , the measures μ_p and the tensors $G^{(p)}$ can additionally depend on \mathbf{x} . The theorem presented below remains valid in the heterogeneous case but for the sake of notational simplicity we shall skip the dependence on \mathbf{x} in the model parameters.

We recall that a function $f: \mathbb{R}_+ \rightarrow \mathbb{R}$ (or $f: \overline{\mathbb{R}_+} \rightarrow \mathbb{R}$) is said to be completely monotonic if it has the derivatives of arbitrary orders and $(-1)^n f^{(n)}(t) \geq 0$ for $n=0, 1, \dots$ and $t > 0$ (or $t \geq 0$) (Widder, 1971). The Laplace transform of the relaxation function of the anisotropic Cole–Cole model $s \rightarrow (1/s) A_p(s)$ is analytic in $\mathbb{C} \setminus \overline{\mathbb{R}_-}$, real and positive for $s > 0$. Furthermore, it tends to 0 for $s \rightarrow \infty$. In the upper-half complex plane $\text{Im } s > 0$

$$\begin{aligned} \text{Im} \frac{1 + a_p (s\tau_p)^{-\alpha_p}}{1 + (s\tau_p)^{-\alpha_p}} &= (1 - a_p) \sin(\alpha_p \phi) \\ &\times \frac{(R\tau_p)^{-\alpha_p}}{|1 + (s\tau_p)^{-\alpha_p}|^2} \geq 0 \end{aligned}$$

where $s = R \exp(i\phi)$. Consequently, by Theorem 5.2.6 in Gripenberg et al. (1990),

$$(1/s) A_p(s) = \int_0^\infty e^{-st} r_p(t) dt$$

where λ_p is locally integrable and completely monotonic. By Bernstein’s theorem (op. cit. or Widder, 1971)

$$r_p(t) = \int_0^\infty e^{-\sigma t} d\mu_p(\sigma), \quad p = 1, \dots, P$$

which implies Eqs. (21) and (22) with $G^{(p)} = E^{(p)} \otimes E^{(p)}$.

The relaxation functions r_p for the relaxation models (12)–(13)

$$a_p - \sum_{n=1}^N b_p^{(n)} \tau_p^{(n)} e^{-t/\tau_p^{(n)}}, \quad t \geq 0 \tag{24}$$

$$a_p t^{-\alpha_p} / \Gamma(1 - \alpha_p), \quad t > 0 \tag{25}$$

with $a_p > \sum_{n=1}^N b_p^{(n)}, b_p^{(n)} > 0$ are obviously completely monotonic on the indicated domains of definition and Eq. (21) holds for these models.

We shall now use Eq. (21) to prove well-posedness of the initial-boundary value problem.

For this purpose we define an auxiliary field

$$\Phi_{kl}(t, \mathbf{x}, \zeta) := \int_{-\infty}^t e^{-\zeta(t-\tau)} v_{k,l}(\tau, \mathbf{x}) d\tau \tag{26}$$

Obviously

$$\sigma_{kl}(t, \mathbf{x}) = \int_0^\infty \Phi_{mn}(t, \mathbf{x}, \zeta) dF_{klmn}(\zeta)$$

Let $\psi_{kl}(t, \mathbf{x}, \zeta) := \zeta \Phi_{kl}(t, \mathbf{x}, \zeta) - [v_{k,l}(t, \mathbf{x}) + v_{l,k}(t, \mathbf{x})]/2$.

The equations of motion can be recast in the following form

$$\rho \dot{v}_k(t, \mathbf{x}) = -\partial \left\{ \int_0^\infty \Phi_{mn}(t, \mathbf{x}, \zeta) dF_{klmn}(\zeta) \right\} / \partial x_l \tag{27}$$

$$\dot{\Phi}_{kl}(t, \mathbf{x}, \zeta) = -\Psi_{kl}(t, \mathbf{x}, \zeta), \quad t, \zeta \geq 0$$

$$\begin{aligned} v_k(0, \mathbf{x}) &= v_k^{(0)}(0, \mathbf{x}); \quad \Phi_{kl}(0, \mathbf{x}, \zeta) \\ &= \Phi_{kl}^{(0)}(\mathbf{x}, \zeta), \quad \zeta \geq 0 \end{aligned}$$

where $\Phi_{kl}^{(0)}(\mathbf{x}, \zeta) := \int_{-\infty}^0 e^{\zeta t} [v_{k,l}^{(0)}(t, \mathbf{x}) + v_{l,k}^{(0)}(t, \mathbf{x})] dt / 2$. Eq. (27) is equivalent to the definition of Φ_{kl} , Eq. (26).

Let $\psi_{kl}^{(0)}(\mathbf{x}, \zeta) := \zeta \Phi_{kl}^{(0)}(\mathbf{x}, \zeta) - [v_{k,l}(0, \mathbf{x}) + v_{l,k}(0, \mathbf{x})]/2$.

Theorem 1. *If G satisfies Eq. (21), the initial history $v_k^{(0)}(t, \mathbf{x})$, $t \leq 0$, satisfies the boundary condition on Γ_1 , $\Phi_{kl}^{(0)}$ is square integrable and*

$$\int_{-\infty}^0 G_{klmn}(-\tau)v_{m,n}^{(0)}(\tau, \mathbf{x})d\tau \text{ is differentiable} \quad (28)$$

then Eq. (27) has a unique solution $v_k \Phi_{kl}$ such that $v_k(0, x) = v_k^{(0)}(0, x)$, $k = 1, 2, 3$.

(Hanyga, 2003c).

It is worth noting that monotonicity and convexity of the stress relaxation functions r_p is crucial for existence and uniqueness. It is not clear whether complete monotonicity is a necessary condition.

6. Regularity

Regularity results can be obtained by the semi-group techniques. They will allow us to distinguish

$$\beta \frac{\text{Im}\{[1 + a_p(i\tau_p\beta)^{-\alpha_p}][1 + (-i\tau_p\beta)^{-\alpha_p}]\}}{\text{Re}\{[1 + a_p(i\tau_p\beta)^{-\alpha_p}][1 + (-i\tau_p\beta)^{-\alpha_p}]\}} \geq \frac{\min\{\tau_p^{-\alpha_p}(1 - a_p)\sin(\pi\alpha_p/2)\beta^{1-\delta(\beta)}\}}{[1 + \max\{a_p\tau_p^{-\alpha_p}\}\beta^{-\varepsilon(\beta)}][1 + \max\{\tau_p^{-\alpha_p}\}\beta^{-\varepsilon(\beta)}]}$$

where

$$\delta(\beta) = \begin{cases} \min\{\alpha_p\} & \text{for } \beta < 1 \\ \max\{\alpha_p\} & \text{for } \beta > 1 \end{cases}$$

and

$$\varepsilon(\beta) = \begin{cases} \max\{\alpha_p\} & \text{for } \beta < 1 \\ \min\{\alpha_p\} & \text{for } \beta > 1 \end{cases}$$

$\gamma(\beta) \sim \text{const} \times \beta^{1-\delta(\beta)}$ for $\beta \rightarrow \infty$ and Theorem 4.3 in Desch and Grimmer (1989a) implies that the solution of Eq. (27) belongs to $\mathcal{C}^\infty(\mathbb{R}_+, H^1(\Omega, \mathbb{R}^3))$. The same criterion also implies finite speed of propagation of disturbances (Prüss, 1993).

For the fractional relaxation model $\beta/\gamma(\beta) = \max\{\cot(\pi\alpha_p/2) | p = 1, \dots, P\}$ provided $0 < \alpha_p < 1$, and the solution is an analytic function of time. For $\alpha_p > 0$ the kernel G relating the delayed stress to the strain has a nonintegrable singularity at 0. The problem is

between various models of relaxation on the basis of the ensuing wavefield properties.

The first regularity results can be obtained from Theorem 4.3 in Desch and Grimmer (1989a). Let

$$U(\beta) := (i\beta/2)[\tilde{G}(i\beta) - \overline{\tilde{G}(i\beta)}] \\ \equiv \sum_{p=1}^6 (1/2) \text{Re} \frac{1 + a_p(i\beta\tau_p)^{\alpha_p}}{1 + (i\beta\tau_p)^{\alpha_p}} E^{(p)} \otimes E^{(p)}$$

$$V(\beta) := (\beta/2)[\tilde{G}(i\beta) + \overline{\tilde{G}(i\beta)}] \\ \equiv \sum_{p=1}^6 (1/2) \text{Im} \frac{1 + a_p(i\beta\tau_p)^{\alpha_p}}{1 + (i\beta\tau_p)^{\alpha_p}} E^{(p)} \otimes E^{(p)}$$

Smoothness of the solutions depends on the asymptotic behavior for large $\beta > 0$ of a function $\gamma(\beta)$ defined by the inequality $\beta V(\beta) - \gamma(\beta)U(\beta) \geq 0$. The left-hand side of this inequality is interpreted as a symmetric operator on \mathcal{L} . Since

parabolic and the propagation speed of disturbances is infinite. The speed of signal propagation can, however, be finite. For example, if $\alpha_p = \alpha$ does not depend on p then the Green's function depends on t, \mathbf{x} through the variable $\xi = x/t^{(1-\alpha)/2}$ (Hanyga, 2002b; Carcione et al., 2002). For $\alpha_p < 0$ the well-posedness fails because the stress relaxation functions r_p are increasing.

7. Numerical methods for the anisotropic Cole–Cole model

In engineering FEM methods in combination with discretized fractional derivatives have been commonly used in modeling of isotropic viscoelastic structures with fractional relaxation (Padovan, 1987), in particular for the Cole–Cole relaxation (Schmidt et al., 2000).

For τ_p independent of $p = 1, \dots, 6$ and a homogeneous medium, the anisotropic Cole–Cole equations can be formulated in terms of fractional derivatives. The fractional derivative formulation immediately

provides several alternative time discretizations. More general time-stepping algorithms are described in Hanyga (2002a). Alternatively, wave propagation can be expressed in terms of a coupled system consisting of the partial differential equations expressing the usual equations of motion and additional ordinary differential equations of fractional order which may be interpreted as relaxation laws (Hanyga, 2003b).

For rational values of α_p , ray-asymptotic methods (based on real ray tracing) can be applied following the methods of Hanyga and Seredyńska (1999a). This is due to the reducibility of the problem to the tracing of a wavefront in real space while the signal shape is represented by convolution with a set of functions representing the evolution of a delta signal. These functions are explicitly calculable for $\alpha_p = 1/2, 1/3, 2/3$ (Hanyga and Seredyńska, 2002). For $\alpha_p = 1/2$, ray tracing requires integration of a single additional transport equation in order to determine the degree of signal spreading and the delay of the signal peak with respect to the wavefront. In contrast, ray-asymptotic methods for the general case of a viscoelastic medium require the use of complex ray tracing in order to capture dispersion and attenuation (Hanyga, 1999a; Hanyga and Seredyńska, 2000).

Essentially identical existence, uniqueness and regularity results have been obtained for linear thermoviscoelasticity with heat conduction (Hanyga, 2003c). In particular, regularity properties depend on the memory kernel and are not affected by thermal effects.

8. Conclusions

Well-posedness has been proved for a class of viscoelastic models constructed by the method of Carcione and Cavallini (1994) with stress relaxation functions enjoying appropriate monotonicity and convexity properties. In this framework the three models of viscoelastic relaxation currently enjoying some popularity in seismic modeling, viz. exponential relaxation (Eq. (24)), fractional relaxation (Eq. (25)) and Cole–Cole relaxation (Eq. (4)), lead to well-posed problems. The first model lacks the smoothing property characteristic of viscosity, the second one is characterized by an infinite speed of propagation of disturbances while

the third combines a finite propagation speed with a smoothing effect of Newtonian viscosity.

In an anisotropic medium the constant Q property cannot be imposed by a constitutive assumption (Hanyga, 2001a) unless all the six relaxation functions are associated with the same Q value (the isotropic case is an exception). The propagation speed is unbounded and perturbations spread immediately to the entire domain while a finite signal speed, resulting from self-similarity, is an attribute of the scalar equation with constant coefficients. It need not be valid for the anisotropic case. On the other hand, the relative advantage of the Cole–Cole model—good matching of experimental data with an economic set of parameters—remains true in the anisotropic case.

It is worth noting that the Cole–Cole law and related viscoelastic models can be expressed in terms of 2–6 internal variables subject to fractional relaxation laws, hence the integral operator representing the memory can be replaced by a set of at most six ordinary differential equations of fractional order (Hanyga, 2003b). For numerical implementation this implies that a generalization of the method developed by Day and Minster (1984), Emmerich and Korn (1987), Simo and Hughes (1998) and Carcione et al. (1988) for exponential relaxation can be applied. This approach can be extended to nonlinear viscoelastic models of rate-dependent hysteresis (Hanyga, 2003b).

Acknowledgements

The paper was prepared during the author's stay at the Division of Engineering and Applied Sciences of the Harvard University. Stimulating remarks by José M. Carcione and Ivan Pšenčík are gratefully acknowledged. Financial support by the Norsk Hydro AS is gratefully acknowledged.

References

- Agrawal, O.P., 1999. An analytical scheme for stochastic dynamical systems containing fractional derivatives. Proceedings of DETC'99, ASME Design Engineering Technical Conferences, September 12–15, 1999, Las Vegas, NV.
- Allard, J.-F., Champoux, Y., 1992. New empirical equations for sound propagation in rigid frame fibrous materials. *J. Acoust. Soc. Am.* 91, 3346–3353.

- Andrade, E.N., 1910. On the viscous flow of metals and allied phenomena. Proc. R. Soc. London 84 (A562).
- Andrade, E.N., 1912. On the validity of the $t^{1/3}$ law of flow of metals. Phil. Mag. 7 (84).
- Bagley, R.L., 1990. On the fractional order initial value problem and its engineering applications. In: Nishimoto, K. (Ed.), Fractional Calculus and its Applications. College of Engineering, Nihon University, Tokyo, pp. 12–20.
- Bagley, R.L., Calico, R.A., 1991. Fractional order state equations for the control of viscoelastically damped structures. J. Guid. Control Dyn. 14, 301–311.
- Bagley, R.L., Torvik, P.J., 1983a. Fractional calculus—a different approach to the analysis of viscoelastically damped structures. AIAA J. 21, 741–748.
- Bagley, R.L., Torvik, P.J., 1983b. Fractional calculus—a different approach to the analysis of viscoelastically damped structures. AIAA J. 21, 741–748.
- Bagley, R.L., Torvik, P.J., 1983c. A theoretical basis for the application of fractional calculus to viscoelasticity. J. Rheol. 27, 201–210.
- Bagley, R.L., Torvik, P.J., 1986. On the fractional calculus model of viscoelastic behavior. J. Rheol. 30, 133–155.
- Batzle, M., Hofmann, R., Han, D.-H., Castagna, J., 2001. Fluids and frequency dependent seismic velocity of rocks. The Leading Edge 20, 168–171.
- Berryman, J.G., Thigpen, L., Chin, R.C., 1988. Bulk elastic wave propagation in partially saturated porous solids. J. Acoust. Soc. Am. 84, 360–373.
- Beyer, H., Kempfle, S., 1995. Definition of physically consistent damping laws with fractional derivatives. ZAMM 75, 623–635.
- Blair, G.W.S., 1944. Survey of General and Applied Rheology. Pitman, New York.
- Boltzmann, L., 1876. Zur Theorie der elastischen Nachwirkung. Ann. Phys. Chem. Erg. Bd. 7.
- Bronskii, A.P., 1941. Aftereffect phenomena in solid bodies. Prikl. Mat. Meh. 5 (1) (In Russian).
- Brunner, H., van der Houwen, P.J., 1986. The Numerical Solution of Volterra Equations. North-Holland, Amsterdam.
- Caputo, M., 1967a. Linear models of dissipation whose Q is almost frequency independent—I. Geophys. J. R. Astron. Soc. 13, 529–539.
- Caputo, M., 1967b. Linear models of dissipation whose Q is almost frequency independent—II. Geophys. J. R. Astron. Soc. 13, 529–539.
- Caputo, M., 1969. Elasticità e dissipazione. Zanichelli, Bologna.
- Caputo, M., Mainardi, F., 1971. Linear models of dissipation in anelastic solids. Riv. Nuovo Cim. (Ser. II) 1, 161–198.
- Caputo, M., Mainardi, F., 1976. New dissipation model based on memory mechanism. Pure Appl. Geophys. 91, 134–147.
- Carcione, J.M., Cavallini, F., 1994. A rheological model for anelastic anisotropic media with applications to seismic wave propagation. Geophys. J. Int. 119, 338–348.
- Carcione, J.M., Kosloff, D., Kosloff, R., 1988. Wave propagation simulation in a linear viscoelastic medium. Geophys. J. R. Astron. Soc. 95, 597–611.
- Carcione, J.M., Cavallini, F., Helbig, K., 1996. Anisotropic attenuation and material symmetry. Acustica-Acta Acustica 84, 495–502.
- Carcione, J.M., Cavallini, F., Mainardi, F., Hanyga, A., 2002. Time-domain seismic modeling of constant- Q wave propagation using fractional derivatives. Pure Appl. Geophys. 159, 1714–1736.
- Cole, K.S., Cole, R.H., 1941. Dispersion and absorption in dielectrics. I: Alternating current characteristics. J. Chem. Phys. 9, 341–351.
- Day, S.M., Minster, J.B., 1984. Numerical simulation of wavefields using a Padé approximant method. Geophys. J. R. Astron. Soc. 78, 105–118.
- Desch, W., Grimmer, R., 1986. Propagation of singularities for integrodifferential equations. J. Differ. Equ. 65, 411–426.
- Desch, W., Grimmer, R., 1989a. Singular relaxation moduli and smoothing in three-dimensional viscoelasticity. Trans. Am. Math. Soc. 314, 381–404.
- Desch, W., Grimmer, R., 1989b. Smoothing properties of linear Volterra integrodifferential equations. SIAM J. Math. Anal. 20, 116–132.
- Diethelm, K., Freed, A.D., 1999. The FracPECE Subroutine for the Numerical Solution of Differential Equations of Fractional Order. Gesellschaft für wissenschaftliche Dataverarbeitung, Göttingen, pp. 57–71.
- Diethelm, K., Freed, A.D., Ford, N., 2002. A predictor–corrector approach to the numerical solution of fractional differential equations. Nonlinear Dyn. 22, 3–22.
- Duffing, G., 1931. Elastizität und Reibung beim Rientrieb. Forsch. Gebiete Ing.wes. 2, 3.
- Dvorkin, J., Nur, A., 1993. Dynamic poroelasticity: a unified model with the squirt and the Biot mechanism. Geophysics 58, 524–533.
- Eldred, B.L., Baker, W.P., Palazzotto, A.N., 1995. Kelvin–Voigt versus fractional derivative model as constitutive relation for viscoelastic materials. AIAA J. 33, 547–550.
- Emmerich, M., Korn, M., 1987. Incorporation of attenuation into time-domain computation of seismic wavefields. Geophysics 52, 1252–1264.
- Enelund, M., Josefson, B.L., 1997. Time-domain finite-element analysis of viscoelastic structures with fractional derivative constitutive equations. AIAA J. 35, 1630–1637.
- Enelund, M., Lesieutre, G.A., 1999. Time-domain modeling of damping using anelastic displacement fields and fractional calculus. Int. J. Solids Struct. 36, 4447–4472.
- Enelund, M., Olsson, P., 1998. Damping described by fading memory—analysis and application to fractional derivative models. Int. J. Solids Struct. 36, 939–970.
- Enelund, M., Fenander, A., Olsson, P., 1997. Fractional integral formulation of constitutive equations of viscoelasticity. AIAA J. 35, 1356–1362.
- Engler, H., 1997. Similarity solutions for a class of hyperbolic integro-differential equations. Differ. Integral Equ. 10, 815–845.
- Fabrizio, M., Morro, A., 1992. Mathematical Problems in Linear Viscoelasticity. SIAM, Philadelphia.
- Fenander, A., 1997. Modal synthesis when modeling damping by use of fractional derivatives. AIAA J. 34, 1051–1058.
- Friedrich, C., 1991. Relaxation and retardation function of the

- Maxwell model with fractional derivatives. *Rheol. Acta* 30, 151–158.
- Friedrich, C., Braun, C., 1992. Generalized Cole–Cole behavior and its rheological relevance. *Rheol. Acta* 31, 309.
- Gaul, L., Klein, P., Kempfle, S., 1989. Impulse response function of an oscillator with fractional derivative in damping description. *Mech. Res. Commun.* 16, 297–305.
- Gaul, L., Klein, P., 1991. Damping description involving fractional derivatives. *Mech. Sys. Signal Process.* 5, 8–88.
- Gemant, A., 1936. A method of analyzing experimental results for elastoviscous bodies. *Physics* 7, 311–317.
- Gemant, A., 1938. On fractional differentials. *Philos. Mag.* 25, 540–549.
- Glöckle, W.G., Nonnenmacher, T.F., 1991. Fractional integral operators and Fox functions in the theory of viscoelasticity. *Macromolecules* 24, 6424–6434.
- Glöckle, W.G., Nonnenmacher, T.F., 1994. Fractional relaxation and the time–temperature superposition principle. *Rheol. Acta* 33, 337–343.
- Gomi, S., Yonezawa, F., 1995. Anomalous relaxation in the Fractal Time Random Walk Model. *Phys. Rev. Lett.* 74, 4125–4128.
- Gripenberg, G., 2001. Non-smoothing in a single conservation law with memory. *Electron. J. Differ. Equ.*, 1–8.
- Gripenberg, G., Londen, S.O., Staffans, O.J., 1990. *Volterra Integral and Functional Equations*. Cambridge Univ. Press, Cambridge.
- Gurevich, B., Lopatnikov, S.L., 1997. Velocity and attenuation of elastic waves in finely layered porous rocks. *Geophys. J. Int.* 121, 933–947.
- Hanyga, A., 1999a. Asymptotic theory of wave propagation in viscoporoelastic media. In: Teng, Y.-C., Shang, E.-C., Pao, Y.-H., Schultz, M.H., Pierce, A.D. (Eds.), *Theoretical and Computational Acoustics '97*. Proc. 3rd Int. Conf. on Computational and Theoretical Acoustics, Newark, NJ, July 14–18, 1997. World-Scientific, Singapore.
- Hanyga, A., 1999b. A fractional differential operator for a generic model of attenuation in a porous medium. A preliminary report. Unpublished, <http://www.geo.uib.no/hjemmesider/andrzej>.
- Hanyga, A., 1999c. Time-stepping for second-order differential hyperbolic equations with fractional time derivatives. Unpublished, <http://www.geo.uib.no/hjemmesider/andrzej>.
- Hanyga, A., 2001a. Scalar and vector models of constant Q wave propagation. Extended Abstracts of the 63rd EAGE Conference and Exhibition, Amsterdam, 11–15 June 2001.
- Hanyga, A., 2001b. Wave propagation in media with singular memory. *Math. Comput. Mech.* 34, 1399–1422.
- Hanyga, A., 2001c. Wave propagation in poroelasticity: equations and solutions. *J. Comput. Acoustics* (in press).
- Hanyga, A., 2002a. An anisotropic Cole–Cole model of seismic attenuation. In: Shang, E.-C., Li, Qihu, Gao, T.F. (Eds.), *Theoretical and Computational Acoustics 2001*. Proc. of the 5th International Conference on Computational and Theoretical Acoustics, Beijing, 21–25 May 2001. World Scientific, New Jersey, pp. 319–333.
- Hanyga, A., 2002b. Multidimensional solutions of time-fractional diffusion-wave equations. *Proc. R. Soc. London A* 458, 933–958.
- Hanyga, A., 2003a. An anisotropic Cole–Cole viscoelastic model of seismic attenuation: well-posedness and numerical methods. *J. Comput. Acoustics*.
- Hanyga, A., 2003b. Internal variable models of viscoelasticity with fractional relaxation laws.
- Hanyga, A., 2003c. Well-posedness and regularity for a class of linear thermo-viscoelastic materials. *Proc. Roy. Soc. London A*.
- Hanyga, A., Rok, V.E., 2000. Wave propagation in micro-heterogeneous porous media: a model based on an integro-differential equation. *J. Acoust. Soc. Am.* 107, 2965–2972.
- Hanyga, A., Sereďyńska, M., 1999a. Asymptotic ray theory in porous and viscoelastic media. *Wave Motion* 30, 175–195.
- Hanyga, A., Sereďyńska, M., 1999b. Some effects of the memory kernel singularity on wave propagation and inversion in poroelastic media: I. Forward modeling. *Geophys. J. Int.* 137, 319–335.
- Hanyga, A., Sereďyńska, M., 2000. Ray tracing in elastic and viscoelastic media. *Pure Appl. Geophys.* 157, 679–717.
- Hanyga, A., Sereďyńska, M., 2002. Asymptotic wavefront expansions in hereditary media with singular memory kernels. *Quart. Appl. Math.* LX, 213–244.
- Havriliak, S., Negami, S., 1967. A complex plane representation of dielectric and mechanical relaxation processes in some polymers. *Polymer* 8, 161–210.
- Helbig, K., 1994. *Foundations of Anisotropy for Exploration Seismics*. Pergamon, London.
- Heymans, N., Bauwens, J.C., 1994. Fractal rheological models and fractional differential equations for viscoelastic behavior. *Rheol. Acta* 33, 219.
- Hrusa, W., Renardy, M., 1988. A model equation for viscoelasticity with a strongly singular kernel. *SIAM J. Math. Anal.* 19, 257–269.
- Johnson, D.L., 2001. Theory of frequency dependent acoustics in patchy-saturated porous media. *J. Acoust. Soc. Am.* 110, 682–694.
- Jones, T.D., 1986. Pore fluids and frequency-dependent wave propagation in rocks. *Geophysics* 51, 1939–1953.
- Jonscher, A.K., 1996. *Universal Relaxation Law*. Chelsea Dielectrics Press, London.
- Kjartansson, E., 1979. Constant Q -wave propagation and attenuation. *J. Geophys. Res.* 84, 4737–4748.
- Klafter, J., Rubin, R.J., Schlesinger, M.F. (Eds.), 1986. *Transport and Relaxation in Random Materials*. World-Scientific, Singapore.
- Koeller, R.C., 1984. Applications of fractional calculus to the theory of viscoelasticity. *J. Appl. Mech.* 51, 299–307.
- Koh, C.G., Kelly, J.M., 1990. Application of fractional derivatives to seismic analysis of base-isolated models. *Earthq. Eng. Struct. Dyn.* 19, 229–241.
- Kohlrausch, R., 1847. *Annal. Phys.* 12, 393.
- Kohlrausch, F., 1863. *Poggendorfer Annal. (Annal. Phys. Chem.)* 119, 337.
- Lokshin, A.A., Rok, V.E., 1978a. Automodel solutions of wave equations with time lag. *Russ. Math. Surv.* 33, 243–244.
- Lokshin, A.A., Rok, V.E., 1978b. Fundamental solutions of the wave equation with delayed time. *Doklady AN SSSR* 239, 1305–1308.
- Lubich, C., 1986. Discretized fractional calculus. *SIAM J. Math. Anal.* 17, 704–719.

- Lubich, C., 1988a. Convolution quadrature and discretized fractional calculus, I–II. *Numer. Math.* 52, 129–145.
- Lubich, C., 1988b. Convolution quadrature and discretized fractional calculus, II. *Numer. Math.* 52, 413–425.
- Mainardi, F., Tomirotti, M., 1997. Seismic pulse propagation with constant Q and stable probability distributions. *Annal. Geofis.* 40, 1311–1328.
- Makris, N., Dargush, G.F., Constantinou, M.C., 1993. Dynamic analysis of generalized viscoelastic fluids. *J. Eng. Mech.* 119, 1663–1679.
- Mbodje, B., Montseny, C., Audunet, J., Benchimol, P., 1994. Optimal control for fractionally damped exible systems. The Proceedings of the Third IEEE Conference on Control Applications, The University of Strathclyde, Glasgow, August 24–26, 1994, pp. 1329–1333.
- Metzler, R., Barkai, E., Klafter, J., 1999. Anomalous diffusion and relaxation close to equilibrium: a fractional Fokker–Planck equation approach. *Phys. Rev. Lett.* 82, 3563–3567.
- Miller, K.S., Ross, B., 1993. *An Introduction to the Fractional Calculus and Fractional Differential Equations*. Wiley, New York.
- Narain, A., Joseph, D.D., 1982. Linearized dynamics for step jumps of velocity and displacement of shearing flows for a simple fluid. *Rheol. Acta* 21, 228–250.
- Nigmatullin, R.R., 1984. On the theory of relaxation with “remnant” memory. *Phys. Stat. Solidi B* 124, 389–393.
- Nigmatullin, R.R., 1986. The realization of the generalized transfer in a medium with fractal geometry. *Phys. Stat. Solidi B* 133, 425–430.
- Norris, A.N., 1986. On the viscodynamic operator in Biot’s theory. *J. Wave-Material Interact.* 1, 365–380.
- Nutting, P.G., 1921. New general law of deformation. *J. Franklin Inst.* 191, 679–685.
- Nutting, P.G., 1943. General stress–strain–time formula. *J. Franklin Inst.* 235, 513–524.
- Nutting, P.G., 1946. Deformation in relation to time, pressure and temperature. *J. Franklin Inst.* 242, 449–458.
- Padovan, J., 1987. Computational algorithms for finite element formulation involving fractional operators. *Comput. Mech.* 2, 275–287.
- Palade, L.I., Verney, V., Atané, P., 1996. A modified fractional model to describe the entire behavior of polybutadienes from flow to glassy regime. *Rheol. Acta* 35, 266–273.
- Podlubny, I., 1998. *Fractional Differential Equations*. Academic Press, San Diego.
- Prüss, J., 1993. *Evolutionary Integral Equations*. Birkhäuser Verlag, Basel.
- Rabotnov, Y.N., 1969. *Creep Problems in Structural Elements*. North-Holland, Amsterdam.
- Rabotnov, Y.N., 1980. *Elements of Hereditary Solid Mechanics*. Mir Publ., Moscow.
- Renardy, M., 1982. Some remarks on the propagation and non-propagation of discontinuities in linearly viscoelastic liquids. *Rheol. Acta* 21, 251–254.
- Ribodetti, A., Hanyga, A., 2004. Some effects of the memory kernel singularity on wave propagation and inversion in poroelastic media: II. Inversion. *Geophys. J. Submitted for publication*.
- Rogers, L., 1983. Operators with fractional derivatives for viscoelastic constitutive relations. *J. Rheol.* 27, 351–372.
- Rossikhin, Y.A., Shitikova, M.V., 1997. Applications of fractional calculus to dynamic problems of linear and nonlinear hereditary mechanisms of solids. *Appl. Mech. Rev.* 50, 15–67.
- Rossikhin, Y.A., Shitikova, M.V., 2000. A new method for solving dynamic problems of fractional derivative viscoelasticity. *Int. J. Eng. Sci.* 39, 149–176.
- Rossikhin, Y.A., Shitikova, M.V., 2001. Analysis of dynamic behaviour of viscoelastic rods whose rheological models contain fractional derivatives of two different orders. *ZAMM* 6, 363–378.
- Ruffet, C., Gueguen, Y., Darot, M., 1991. Complex conductivity measurements and fractal nature of porosity. *Geophysics* 56, 758–768.
- Rzhanitsyn, A.R., 1949. *Some Problems of the Mechanics of Systems That are Deformed in Time*. Gostekhizdat, Moscow.
- Rzhanitsyn, A.R., 1968. *Theory of Creep*. Stroiizdat, Moscow. In Russian.
- Schiessel, H., Blumen, A., 1993. Hierarchical analogues to fractional relaxation equations. *J. Phys. A: Math. Gen.* 26, 5057–5069.
- Seredyńska, M., Hanyga, A., 2000. Nonlinear Hamiltonian equations with fractional damping. *J. Math. Phys.* 41, 2135–2156.
- Simo, J.C., Hughes, T.J.R., 1998. *Computational Inelasticity*. Springer, New York.
- Slonimsky, G.L., 1939. On the laws of deformation of real materials. *J. Theor. Phys.* 9 (20) (In Russian).
- Slonimsky, G.L., 1961. On the laws of deformation of visco-elastic polymeric bodies. *DAN SSSR* 140 (2) (In Russian).
- Slonimsky, G.L., 1967. Laws of mechanical relaxation processes in polymers. *J. Polym. Sci.* C16, 1667–1672.
- Soula, M., Chevalier, Y., 1998. La dérivée fractionnaire en rhéologie des polymères—Application aux comportements élastiques et viscoélastiques linéaires et non-linéaires des élastomères. *ESAIM: Proceedings Fractional Differential Systems: Models, Methods and Applications*, vol. 5, pp. 193–204.
- Soula, M., Vinh, T., Chevalier, Y., 1997. Transient responses of polymers and elastomers deduced from harmonic responses. *J. Sound Vib.* 205, 185–203.
- Stinson, M.R., Champoux, Y., 1992. Propagation of sound and the assignment of shape factors in model porous materials having simple pore geometries. *J. Acoust. Soc. Am.* 91, 685–695.
- Strick, E., 1984. Implications of Jeffreys–Lomnitz transient creep. *J. Geophys. Res.* 89, 437–451.
- Suarez, L., Shokooh, A., 1995. Response of systems with damping materials modeled using fractional derivatives. *Appl. Mech. Rev.* 48, S118–S126.
- Suarez, L., Shokooh, A., 1997. An eigenvector expansion method for the equation of motion containing fractional derivatives. *ASME J. Appl. Mech.* 64, 629–635.
- Szabo, T.L., 1994. Time domain wave equations for lossy media obeying a frequency power law. *J. Acoust. Soc. Am.* 96, 491–500.
- Szabo, T.L., 1995. Causal theories and data for acoustic attenuation obeying a frequency power law. *J. Acoust. Soc. Am.* 97, 14–24.
- Szabo, T.L., Wu, J., 2000. A model for longitudinal and shear wave propagation in viscoelastic media. *J. Acoust. Soc. Am.* 107, 2437–2446.

- Taherian, M.R., Kenyon, W.E., Safinya, K.A., 1990. Measurement of dielectric response of water-saturated rocks. *Geophysics* 55, 1530–1541.
- Torvik, P.J., Bagley, R.L., 1983. On the appearance of the fractional derivative in the behavior of real material. *J. Appl. Mech.* 51, 294–298.
- Torvik, P.J., Bagley, R.L., 1984. On the appearance of fractional derivative in the behavior of real materials. *J. Appl. Mech.* 51, 294–298.
- Torvik, P.J., Bagley, R.L., 1985. Fractional calculus in the transient analysis of viscoelastically damped structures. *AIAA J.* 23, 918–925.
- Truesdell, C., 1972. *A First Course in Rational Mechanics*. John Hopkins University, Baltimore, MA.
- Tutuncu, A.N., Podio, A.L., Gregory, A.R., Sharma, M.M., 1998. Nonlinear viscoelastic behavior of sedimentary rocks: Part I. Effect of frequency and strain amplitudes. *Geophysics* 63, 184–194.
- Weron, K., Kotulski, M., 1996. On the Cole–Cole relaxation function and related Mittag–Leffler distribution. *Phys. A* 232, 180–188.
- Widder, D.V., 1946. *The Laplace Transform*. Princeton Univ. Press, Princeton.
- Widder, D.V., 1971. *An Introduction to Transformation Theory*. Academic Press, New York.
- Williams, G., Watts, D.C., 1970. Nonsymmetrical dielectric relaxation behaviour arising from a simple empirical decay function. *Trans. Faraday Soc.* 66, 80–85.
- Wilson, D.K., 1992. Relaxation-matched modelling of propagation through porous media, including fractal pore structure. *J. Acoust. Soc. Am.* 94, 1136–1145.
- Yosida, K., 1974. *Functional Analysis*, 4th ed. Springer-Verlag, Berlin.
- Yuan, L., Agrawal, O.P., 1998. A numerical scheme for dynamic systems containing fractional derivatives. *Proceedings of DETC'98, ASME Design Engineering Technical Conferences*, September 13–16, 1998, Atlanta, GA.